

Problem 8.2

First find the \vec{E} and \vec{H} -fields associated with the TEM-mode in the region between two concentric cylinders of radii a, b :

\Rightarrow Recall that \vec{E} obeys the equations of 2-dim^l electrostatics, namely

$$\nabla_t \times \vec{E} = 0, \quad \nabla_t \cdot \vec{E} = 0$$

Let's use the azimuthal symmetry to write the 2D scalar potential as

$$\Phi(\rho, \phi) \rightarrow \Phi(\rho), \quad \text{and } \vec{E} = -\nabla_t \Phi$$

$$\text{Then } \nabla_t^2 \Phi(\rho) = 0 = \frac{1}{\rho} \frac{\partial}{\partial \rho} \left(\rho \frac{\partial \Phi}{\partial \rho} \right) + \frac{1}{\rho^2} \frac{\partial^2 \Phi}{\partial \phi^2}$$

$$\Rightarrow \rho \frac{\partial \Phi}{\partial \rho} = A, \quad \text{for some constant } A_1$$

$$\text{and } \frac{\partial \Phi}{\partial \rho} = \frac{A_1}{\rho} \Rightarrow \Phi = A_1 \ln \rho + A_2$$

Setting the potential difference equal to V_0 ,

$$\text{i.e. } V_0 \equiv \Phi(b) - \Phi(a) = A_1 \ln \frac{b}{a}, \Rightarrow A_1 = \frac{V_0}{\ln \frac{b}{a}}$$

whereby
$$\vec{E} = -\frac{A_1}{\rho} \hat{\rho} = -\frac{V_0}{\ln \frac{b}{a}} \frac{\hat{\rho}}{\rho}$$

and from (8.28),
$$\vec{H} = \left(\frac{\epsilon}{\mu}\right)^{1/2} \hat{z} \times \vec{E}$$

$$\Rightarrow \vec{H} = -\left(\frac{\epsilon}{\mu}\right)^{1/2} \frac{V_0}{\ln \frac{b}{a}} \frac{1}{\rho} \hat{\phi} \equiv -H_0 \frac{a}{\rho} \hat{\phi}$$

And of course both \vec{E} and \vec{H} have an implied factor of $e^{i(kz - \omega t)}$,

$$\text{where } k = \omega \sqrt{\mu \epsilon}$$

(8.2) (a) The t -averaged power flow down the waveguide (transmission line) is

$$P = \int_A \frac{1}{2} \vec{E} \times \vec{H}^* \cdot d\vec{a} = \frac{1}{2} \frac{|V_0|^2}{\left(\ln \frac{b}{a}\right)^2} \left(\frac{\epsilon}{\mu}\right)^{1/2} 2\pi \int_a^b \frac{\rho d\rho}{\rho^2}$$

$$\Rightarrow P = \frac{\pi |V_0|^2}{\left(\ln \frac{b}{a}\right)^2} \left(\frac{\epsilon}{\mu}\right)^{1/2} \ln \frac{b}{a}$$

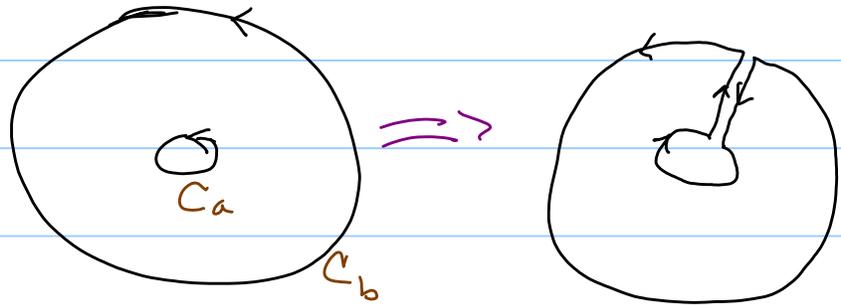
or if we denote $H_0 \equiv \left(\frac{\epsilon}{\mu}\right)^{1/2} \frac{V_0}{\ln \frac{b}{a}} \frac{1}{a}$

$$\Rightarrow P = \pi a^2 \left(\frac{\mu}{\epsilon}\right)^{1/2} |H_0|^2 \ln \frac{b}{a}$$

8.2(b) Now, from Sec. 8.1 and Eq. 8.58,

$$-\frac{dP}{dz} = \frac{1}{2\sigma\delta} \oint_C |\hat{n} \times \vec{H}| dl$$

\Rightarrow Here the closed contour boundary of the area A has two disconnected parts:



$$\begin{aligned} \Rightarrow -\frac{dP}{dz} &= \frac{1}{2\sigma\delta} \left(\oint_{C_a} |\hat{n} \times \vec{H}|^2 dl + \oint_{C_b} |\hat{n} \times \vec{H}|^2 dl \right) \\ &= \frac{1}{2\sigma\delta} \left(2\pi a |H_0|^2 \frac{a^2}{a^2} + 2\pi b |H_0|^2 \frac{a^2}{b^2} \right) \end{aligned}$$

$$\Rightarrow -\frac{dP}{dz} = \frac{\pi |H_0|^2}{\sigma\delta} \left(\frac{1}{a} + \frac{1}{b} \right) a^2$$

Thus in the loss equation $P(z) = P_0 e^{-2\gamma z}$, we have

$$\gamma = \frac{-dP/dz}{2P} = \frac{\pi |H_0|^2 \left(\frac{1}{a} + \frac{1}{b} \right) \frac{a^2}{\sigma\delta}}{2\pi a^2 |H_0|^2 \left(\frac{\mu}{\epsilon} \right)^{1/2} \ln \frac{b}{a}}$$

or

$$\gamma = \frac{1}{2\sigma\delta} \left(\frac{\epsilon}{\mu} \right)^{1/2} \frac{\left(\frac{1}{a} + \frac{1}{b} \right)}{\ln \frac{b}{a}}$$

8.2c The current flowing on the conductor surfaces is, from (8.14):

$$\vec{K}_{eff} = \hat{n} \times \vec{H}_{||} = \begin{cases} (-\hat{\rho}) \times H_{\phi} \hat{\phi}, & \rho = b \\ (+\hat{\rho}) \times H_{\phi} \hat{\phi}, & \rho = a \end{cases}$$

$$= -H_{\phi}(\rho=b) \hat{z}, \quad \text{at outer surface}$$

$$= H_{\phi}(\rho=a) \hat{z}, \quad \text{at inner surface}$$

$$\Rightarrow \vec{I}_{outer} = \int_{\rho=b}^{\rho=b} \vec{K}_{eff} dl = \hat{z} \int_0^{2\pi} [-H_0 \frac{a}{\rho}] a d\phi = 2\pi a H_0 \hat{z}$$

whereas

$$\vec{I}_{inner} = \int_{\rho=a}^{\rho=a} \vec{K}_{eff} dl = \hat{z} \int_0^{2\pi} [+H_0 \frac{a}{\rho}] b d\phi$$

$$= -2\pi H_0 a \hat{z}$$

So the inner and outer conductors carry equal and opposite currents, as is expected and desired, namely $I = 2\pi a H_0$.

The transmission line impedance is then

$$Z_0 = \frac{V}{I} = V_0 \left[\left(\frac{\epsilon}{\mu} \right)^{1/2} \frac{V_0 \frac{2\pi a}{a}}{\ln \frac{b}{a}} \right]^{-1}$$

or

$$Z_0 = \left(\frac{\mu}{\epsilon} \right)^{1/2} \frac{\ln \frac{b}{a}}{2\pi}$$

(8.2 d) The time-averaged power loss per unit length can be related to the resistance per unit length $\frac{dR}{dz}$:

$$\frac{dP_{\text{loss}}}{dz} = \frac{|I_0|^2}{2} \frac{dR}{dz}$$

$$\Rightarrow \frac{dR}{dz} = \frac{2}{|I_0|^2} \frac{dP_{\text{loss}}}{dz} = \frac{2\pi |H_0|^2 \left(\frac{1}{a} + \frac{1}{b}\right) \frac{1}{\sigma \delta}}{\frac{\epsilon}{\mu} |V_0|^2 \frac{(2\pi)^2}{\left(\ln \frac{b}{a}\right)^2}}$$

or plugging in $H_0 = \left(\frac{\epsilon}{\mu}\right)^{1/2} \frac{V_0}{a \ln \frac{b}{a}}$

$$\Rightarrow \frac{dR}{dz} = \frac{\frac{\epsilon}{\mu} \frac{1}{a^2} \left(\frac{1}{a} + \frac{1}{b}\right) a^2}{\frac{\epsilon}{\mu} \sigma \delta (2\pi)} = \frac{1}{2\pi \sigma \delta} \left(\frac{1}{a} + \frac{1}{b}\right) = \frac{dR}{dz}$$

And the time-averaged magnetic energy per unit length is

$$\frac{dW_B}{dz} = \frac{1}{4} \int \vec{B} \cdot \vec{H}^* da$$

We must evaluate this both between the conductors and inside each conductor.

i.e. $dW_B^{(\text{between})}$

$$\frac{dW_B}{dz} = \frac{\mu}{4} 2\pi \int_a^b \rho d\rho |\vec{H}|^2 = \frac{\mu\pi}{2} \int_a^b \frac{\epsilon |V_0|^2}{\mu (\ln \frac{b}{a})^2} \frac{d\rho}{\rho}$$

$$= \frac{\epsilon\pi}{2} \frac{|V_0|^2}{(\ln \frac{b}{a})^2} \ln \frac{b}{a} = \frac{\epsilon\pi}{2} \frac{|V_0|^2}{\ln \frac{b}{a}}$$

while the energy stored within the INNER conductor is found using:

$$\vec{H}_c^{\text{in}} = -H_0 \phi e^{-\frac{(a-\rho)}{\delta}} e^{i(a-\rho)/\delta}$$

$$\Rightarrow \frac{dW_B^{\text{innen}}}{dz} = \frac{\mu_c}{4} 2\pi |H_0|^2 \int_0^a \rho e^{-2(a-\rho)/\delta} d\rho$$

$$= \frac{\mu_c \pi \delta a}{4} |H_0|^2$$

$$\frac{\delta}{4} (2a - \delta + \delta e^{-2a/\delta})$$

$$= \frac{\mu_c \pi \delta a}{4} \frac{\epsilon}{\mu} \frac{|V_0|^2}{(\ln \frac{b}{a})^2} \frac{1}{a^2} = \frac{\pi \epsilon \delta}{4a} \frac{|V_0|^2}{(\ln \frac{b}{a})^2} \frac{\mu_c}{\mu} \approx \frac{\delta a}{2} \text{, if } \delta \ll a$$

while that stored in the outer conductor is:

$$\frac{dW_B^{\text{outer}}}{dz} = \frac{\mu_c}{4} |H_0|^2 \frac{a^2}{b^2} \int_b^\infty (2\pi\rho) e^{-2(\rho-b)/\delta} d\rho$$

$$= \frac{\mu_c \pi b \delta}{4} \frac{a^2}{b^2} |H_0|^2$$

$$\frac{2\pi}{4} (2b\delta + \delta^2) \approx \pi b \delta, \text{ if } \delta \ll b$$

$$= \frac{\pi \epsilon \delta}{4b} \frac{|V_0|^2}{(\ln \frac{b}{a})^2} \frac{\mu_c}{\mu}$$

$$\Rightarrow \frac{1}{4} \frac{dL}{dz} |I_0|^2 = |V_0|^2 \left\{ \frac{\epsilon \pi}{2 \ln \frac{b}{a}} + \frac{\pi \epsilon \delta}{4 (\ln \frac{b}{a})^2} \left(\frac{1}{a} + \frac{1}{b} \right) \right\}$$

$$\Rightarrow \frac{dL}{dz} = \frac{4}{(2\pi)^2} \left\{ \frac{\epsilon \pi}{2 \ln \frac{b}{a}} + \frac{\pi \epsilon \delta}{4 (\ln \frac{b}{a})^2} \left(\frac{1}{a} + \frac{1}{b} \right) \frac{\mu_c}{\mu} \right\}$$

or

$$\frac{dL}{dz} = \frac{\mu}{2\pi} \ln \frac{b}{a} + \frac{\mu_c \delta}{4\pi} \left(\frac{1}{a} + \frac{1}{b} \right)$$

Problem 8.4

We have a hollow cylinder of inner radius R .

The 2D wave equation to be satisfied is

$$(\nabla_t^2 + \gamma_\lambda^2) \Psi_\lambda = 0, \text{ where } \gamma_\lambda^2 = \mu \epsilon \omega^2 - k^2$$

and $\omega_\lambda^2 = \frac{\gamma_\lambda^2}{\mu \epsilon}$

The solutions must be:

$$R(\rho) e^{im\phi} = J_m(\gamma_\lambda \rho) e^{im\phi}$$

(a) TM modes - these obey $\Psi_\lambda(R, \phi) = 0$,

so we can write $\gamma_\lambda = \frac{\chi_{mn}}{R}$

where χ_{mn} is the n th root of $J_m(\chi_{mn}) = 0$

By consulting a table of Bessel zeros, or Mathematica, the lowest 5 TM modes are seen to be:

m	n	χ_{mn}	$\omega_{mn} = \frac{c}{R} \chi_{mn}$	$\frac{\omega_{mn}}{\omega_{01}} = \frac{\chi_{mn}}{\chi_{01}}$
0	1	2.405		1
1	1	3.832		1.593
2	1	5.136		2.136
0	2	5.520		2.295
3	1	6.380		2.653

Similarly, the TE modes obey $\frac{\partial \Psi}{\partial n}(R, \phi) = 0$

$$\Rightarrow J'_m(\gamma_\lambda R) = 0$$

Denote $\chi'_{mn} = n$ th zero of $J'_m(\chi'_{mn}) = 0$

m	n	x_{mn}	$\frac{x_{mn}}{x_{11}}$
1	1	1.841	1
2	1	3.054	1.659
0	1	3.832	2.081
3	1	4.201	2.282
4	1	5.3175	2.888

Thus, the dominant mode has cutoff frequency equal to

$$\omega_{11}^{TE} = 1.841 \frac{c}{R}$$

(8.4b) The relevant equations needed here are 8.59, 8.51, 8.57

Now, for the lowest TM mode $(m,n) = (0,1)$

$$\Rightarrow \beta_{01}^{TM} = - \frac{dP/dz}{2P} = \frac{\frac{1}{2\sigma\delta} \left(\frac{\omega}{\omega_\lambda}\right)^2 \frac{1}{\mu^2 \omega_\lambda^2} \oint_C \left|\frac{\partial\psi}{\partial n}\right|^2 dl}{\frac{\epsilon}{2\sqrt{\mu\epsilon}} \left(\frac{\omega}{\omega_\lambda}\right)^2 \left(1 - \frac{\omega_\lambda^2}{\omega^2}\right)^{1/2} \int_A |\psi|^2 da} \cdot \frac{1}{2}$$

$$\text{or } \beta_{01}^{TM} = \frac{c \oint_C \left|\frac{\partial\psi}{\partial n}\right|^2 dl}{2\sigma\delta \mu \omega_\lambda^2 \left(1 - \frac{\omega_\lambda^2}{\omega^2}\right)^{1/2} \int_A |\psi|^2 da}$$

and $\psi = J_m\left(\frac{x_{mn}\rho}{R}\right) e^{im\phi}$

$$\text{So } \oint_C \left|\frac{\partial\psi}{\partial n}\right|^2 dl = 2\pi R \left| \frac{\partial}{\partial \rho} J_m\left(\frac{x_{mn}\rho}{R}\right) \right|_{\rho=R}^2$$

$$= \frac{2\pi R}{R^2 x_{mn}^2} \left| \frac{R}{x_{mn}} \frac{\partial}{\partial \rho} J_m\left(\frac{x_{mn}\rho}{R}\right) \right|_{\rho=R}^2 \quad 09$$

$$= \frac{2\pi x_{mn}^2}{R} \left| \frac{\partial}{\partial X} J_m(X) \right|_{X \rightarrow x_{mn}}^2$$

whereas,

$$\int_A |\Psi|^2 da = 2\pi \int_0^R \rho d\rho \left| J_m\left(\frac{x_{mn}\rho}{R}\right) \right|^2$$

$$= 2\pi \frac{R^2}{2} \left\{ J_m(x_{mn})^2 - J_{m-1}(x_{mn}) J_{m+1}(x_{mn}) \right\}$$

$$\text{so } \beta_{01}^{TM} = \frac{c 2 (x_{01}^2 / R^3)}{2\sigma\delta\mu\omega_{01}^2 \left(1 - \frac{\omega_{01}^2}{\omega^2}\right)^{1/2}} \frac{|J_m'(x_{mn})|^2}{\left\{ J_m(x_{mn})^2 - J_{m-1}(x_{mn}) J_{m+1}(x_{mn}) \right\}}$$

$$\text{so } \beta_{01}^{TM} = \frac{c}{\sigma\delta\mu R} \frac{x_{01}^2}{R^2} \frac{1}{\omega_{01}^2 \left(1 - \frac{\omega_{01}^2}{\omega^2}\right)^{1/2}}$$

$$\text{but } \frac{x_{01}^2}{R^2} = \gamma_{01}^2 = \frac{\omega_{01}^2}{c^2}$$

$$\Rightarrow \beta_{01}^{TM} = \frac{1}{\sigma\delta\mu c R} \left(1 - \frac{\omega_{01}^2}{\omega^2}\right)^{-1/2}$$

or to make the full dependence on ω explicit,
use

$$\delta \equiv \left(\frac{2}{\mu_c \omega \sigma}\right)^{1/2} = \delta_\lambda \left(\frac{\omega_\lambda}{\omega}\right)^{1/2} \rightarrow \delta_{01} \left(\frac{\omega_{01}}{\omega}\right)^{1/2}$$

$$\Rightarrow \beta_{01}^{TM} = \frac{\sqrt{\mu\epsilon}}{\sigma\delta_{01}\mu R} \frac{(\omega/\omega_{01})^{1/2}}{\left(1 - \frac{\omega_{01}^2}{\omega^2}\right)^{1/2}}$$

Now for the lowest TE mode (1,1), where the attenuation constant is given by

$$\beta_{11}^{TE} = \frac{1}{2\sigma\delta} \left(\frac{\omega}{\omega_\lambda}\right)^2 \oint_C \left[\left(1 - \frac{\omega_\lambda^2}{\omega^2}\right) \frac{1}{\mu\epsilon\omega_\lambda^2} |\hat{n} \times \nabla_\epsilon \psi|^2 + \frac{\omega_\lambda^2}{\omega^2} |\psi|^2 \right] dl$$

$$\frac{\mu}{2\sqrt{\mu\epsilon}} \left(\frac{\omega}{\omega_\lambda}\right)^2 \left(1 - \frac{\omega_\lambda^2}{\omega^2}\right)^{1/2} \int_A |\psi|^2 da \quad (2)$$

The only new nontrivial integral still to evaluate is in the numerator, with $\psi = J_m\left(\frac{x'_{mn}\rho}{R}\right) e^{im\phi}$:

$$\oint_C dl |\hat{n} \times \nabla_\epsilon \psi|^2 = \int_0^{2\pi} R d\phi \left| \frac{ime^{im\phi} J_m(x'_{mn})}{R} \right|^2$$

$$= \frac{2\pi m^2}{R} J_m^2(x'_{mn}) \xrightarrow{(1,1)} \frac{2\pi}{R} J_1^2(x'_{11})$$

and thus

$$\beta_{11}^{TE} = \frac{\left(1 - \frac{\omega_{11}^2}{\omega^2}\right) \frac{1}{\mu\epsilon\omega_{11}^2} \frac{2\pi}{R} J_1^2(x'_{11}) + \frac{\omega_{11}^2}{\omega^2} J_1^2(x'_{11}) (2\pi R)}{2\mu c \left(1 - \frac{\omega_{11}^2}{\omega^2}\right)^{1/2} \sigma\delta \pi R^2 \left\{ J_1^2(x'_{11}) - J_0(x'_{11}) J_2(x'_{11}) \right\}}$$

Now note that $\frac{J_1^2(x'_{11})}{J_1^2(x'_{11}) - J_0(x'_{11}) J_2(x'_{11})} = 1.418\dots$

and as before

$$\delta = \delta_\lambda \left(\frac{\omega_\lambda}{\omega}\right)^{1/2}$$

$$\Rightarrow \beta_{11}^{TE} = \frac{\sqrt{\mu\epsilon} \cdot 1.418 \cdot (\omega/\omega_{11})^{1/2}}{\sigma\delta_\lambda \mu R} \left\{ \underbrace{\left(\frac{R^{-2}c^2}{\omega_{11}^2}\right)}_{\substack{\text{" } r^{-2} \\ x_{11}}} \left(1 - \frac{\omega_{11}^2}{\omega^2}\right) + \frac{\omega_{11}^2}{\omega^2} \right\}$$

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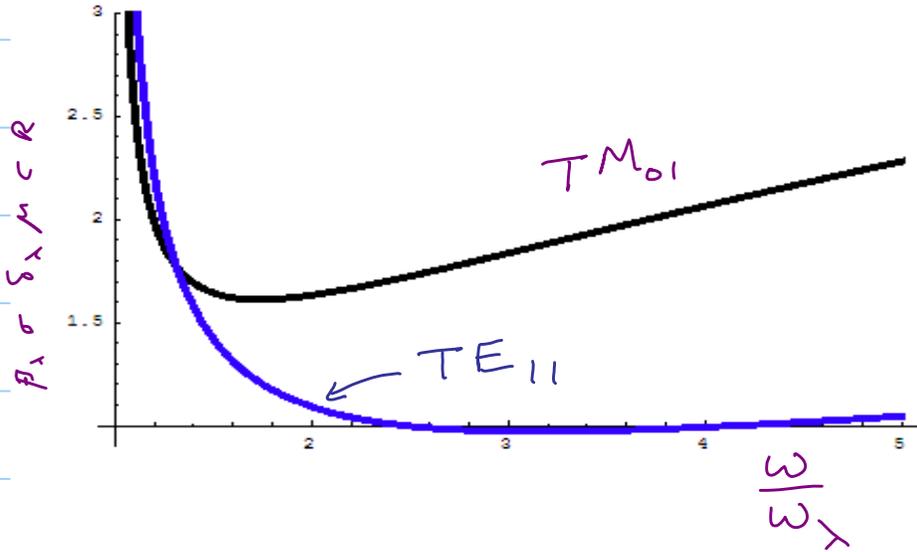
Plot of the lowest TM and TE mode decay parameter:

$$TM_{plot} = \text{Plot}\left[\sqrt{\frac{w}{w_0}} \frac{1}{\sqrt{1 - w_0^2/w^2}}, \{w, w_0 * 1.01, w_0 * 5\}, \text{PlotStyle} \rightarrow \text{Thickness}[0.01]\right] /. w_0 \rightarrow 1;$$

$$TE_{plot} = \text{Plot}\left[\sqrt{\frac{w}{w_0}} \frac{1}{\sqrt{1 - w_0^2/w^2}} 1.418 \left(\frac{1}{(1.84118)^2} (1 - w_0^2/w^2) + \frac{w_0^2}{w^2}\right), \{w, w_0 * 1.01, w_0 * 5\},\right.$$

$$\left. \text{PlotStyle} \rightarrow \{\text{Thickness}[0.01], \text{Hue}[0.7]\}\right] /. w_0 \rightarrow 1;$$

Show[TMplot, TEplot, PlotRange -> {0.9, 3}]:



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Evaluation of $\int_0^R \rho d\rho J_m(x'_{11} \frac{\rho}{R}) J_m(x'_{11} \frac{\rho}{R}) \equiv 1$
 let $y \equiv \rho/R$

$$\Rightarrow \Lambda = \lim_{\bar{x} \rightarrow x'_{11}} R^2 \int_0^1 y dy J_m(x'_{11} y) J_m(\bar{x} y)$$

where $J'_m(x) \Big|_{x=x'_{11}} = 0$

But let's call L_y the Bessel function's Sturm-Liouville operator, i.e.

$$L_y = -\frac{1}{y} \frac{d}{dy} y \frac{d}{dy} + \frac{m^2}{y^2}, \text{ then the Bessel fcn's obey}$$

$$L_y J_m(xy) = x^2 J_m(xy)$$

Then the following identity is useful:

$$\Lambda = \lim_{\bar{x} \rightarrow x'_{11}} R^2 \int_0^1 y dy \frac{J_m(x'_{11} y) L_y J_m(\bar{x} y) - J_m(\bar{x} y) L_y J_m(x'_{11} y)}{\bar{x}^2 - x'^2_{11}}$$

and plugging in the differential operator here gives:

$$\Lambda = \lim_{\bar{x} \rightarrow x'_{11}} R^2 \int_0^1 y dy \left\{ \frac{J_m(\bar{x} y)}{y} \frac{d}{dy} \left(y \frac{d J_m(x'_{11} y)}{dy} \right) - \frac{J_m(x'_{11} y)}{y} \frac{d}{dy} \left(y \frac{d J_m(\bar{x} y)}{dy} \right) \right\} \frac{1}{\bar{x}^2 - x'^2_{11}}$$

Now integrate both terms by parts, giving

$$\Lambda = \lim_{\bar{x} \rightarrow x'_{ii}} R^2 \int_0^1 dy \left[\frac{dJ_m(x'_{ii}y)}{dy} y \frac{dJ_m(\bar{x}y)}{dy} - \frac{dJ_m(\bar{x}y)}{dy} y \frac{dJ_m(x'_{ii}y)}{dy} \right]$$

$$\frac{\bar{x}^2 - x'^2_{ii}}{2}$$

$$+ \lim_{\bar{x} \rightarrow x'_{ii}} R^2 \frac{y J_m(\bar{x}y) \frac{dJ_m(x'_{ii}y)}{dy} - y J_m(x'_{ii}y) \frac{dJ_m(\bar{x}y)}{dy}}{\bar{x}^2 - x'^2_{ii}} \Big|_0^1$$

\Rightarrow the surface term is all that remains, and we must evaluate this \propto limit: set $\bar{x} = x'_{ii} + \delta$ with $\delta \ll 1$, then

$$J_m(\bar{x}y) \approx J_m(x'_{ii}y) + \frac{dJ_m(\bar{x}y)}{d\bar{x}} \Big|_{\bar{x}=x'_{ii}} \delta$$

$$\text{and } \frac{dJ_m(\bar{x}y)}{dy} \approx \frac{dJ_m(x'_{ii}y)}{dy} + \delta \frac{d}{d\bar{x}} \frac{dJ_m(\bar{x}y)}{dy} \Big|_{\bar{x}=x'_{ii}}$$

$$\Lambda = R^2 \lim_{\delta \rightarrow 0} \frac{\delta}{2x'_{ii}} \left[\frac{dJ_m(x'_{ii}y)}{dx'_{ii}} \frac{dJ_m(x'_{ii}y)}{dy} - J_m(x'_{ii}y) \frac{d}{dx'_{ii}} \frac{dJ_m(x'_{ii}y)}{dy} \right]_{y=1}$$

$$\text{So call } J'_m(u) \equiv \frac{d}{du} J_m(u)$$

$$\Rightarrow \frac{dJ_m(x'_{ii}y)}{dx'_{ii}} \Big|_{y=1} = y \frac{dJ'_m(u)}{du} \Big|_{u=x'_{ii}} = 0$$

$$\text{and } \frac{d}{dx'_{ii}} \frac{dJ_m(x'_{ii}y)}{dy} = \frac{d}{dx'_{ii}} x'_{ii} \frac{d}{d(x'_{ii}y)} J_m(x'_{ii}y)$$

$$= x'_{ii} y \frac{d^2 J_m(u)}{du^2} \Big|_{u=x'_{ii}} \quad \text{since } \frac{dJ_m(u)}{du} \Big|_{u=x'_{ii}} = 0$$

$$\Rightarrow \Lambda = -\frac{R^2}{2} \left[J'_m(u) J''_m(u) \right]_{u=x'_{ii}}$$