

Sec. 7.3 Reflection, refraction at an interface

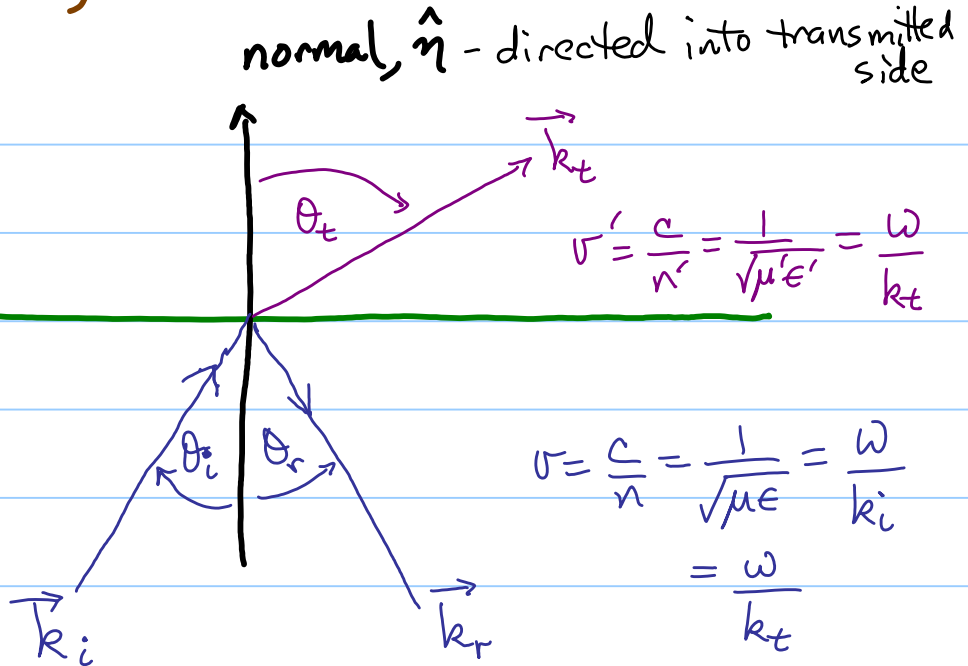
transmitted side

$$\mu', \epsilon', n' = \left(\frac{\mu' \epsilon'}{\mu_0 \epsilon_0} \right)^{1/2}$$

boundary

incident side

$$\mu, \epsilon, n = \left(\frac{\mu \epsilon}{\mu_0 \epsilon_0} \right)^{1/2}$$



The 3 arrows here correspond to 3 plane waves:

Incident

$$\vec{E}_i = \vec{E}_{oi} e^{i(\vec{k}_i \cdot \vec{x} - \omega t)}$$

$$\vec{B}_i = \sqrt{\mu \epsilon} \hat{k}_i \times \vec{E}_i = \frac{n}{c} \hat{k}_i \times \vec{E}_i$$

Reflected

$$\vec{E}_r = \vec{E}_{or} e^{i(\vec{k}_r \cdot \vec{x} - \omega t)}$$

$$\vec{B}_r = \frac{n}{c} \hat{k}_r \times \vec{E}_r$$

Transmitted

$$\vec{E}_t = \vec{E}_{ot} e^{i(\vec{k}_t \cdot \vec{x} - \omega t)}$$

$$\vec{B}_t = \frac{n'}{c} \hat{k}_t \times \vec{E}_t$$

and of course, here $k_i = k_r = \frac{n\omega}{c}$

while $k_t = \frac{n'\omega}{c} = \frac{n'}{n} k_i = \frac{n'}{n} k_r$

- One must have the same ω in all 3 plane waves in order to satisfy BC's at all times.

- Also, assuming both media are homogeneous, symmetry demands that all 3 wavevectors, $\vec{k}_i, \vec{k}_r, \vec{k}_t$ (+ the normal $\hat{n}$) must lie in a single plane, taken here to be the $z=0$ plane

- In order for the imposed boundary conditions to hold along the entire planar interface, we must also have:

$$e^{i\vec{k}_i \cdot \vec{x}} \Big|_{z=0} = e^{i\vec{k}_r \cdot \vec{x}} \Big|_{z=0} = e^{i\vec{k}_t \cdot \vec{x}} \Big|_{z=0}$$

$$\Rightarrow \vec{k}_i \cdot \vec{x} \Big|_{z=0} = \vec{k}_r \cdot \vec{x} \Big|_{z=0} = \vec{k}_t \cdot \vec{x} \Big|_{z=0}$$

$$\Rightarrow k_i \sin \theta_i = k_r \sin \theta_r = k_t \sin \theta_t \quad \left(\begin{array}{l} k\text{-components} \\ \text{along surface} \\ \text{are equal} \end{array} \right)$$

$$\Rightarrow \boxed{\theta_i = \theta_r} \quad \begin{array}{l} \text{angle of incidence} \\ = \text{angle of reflection} \end{array} \quad \left(\begin{array}{l} \text{since} \\ k_i = k_r \end{array} \right)$$

$$\text{and since } k_i = \frac{n\omega}{c}, \quad k_t = \frac{n'\omega}{c}$$

$$\Rightarrow \boxed{n \sin \theta_i = n' \sin \theta_t} \leftarrow \begin{array}{l} \text{Snell's law} \\ \text{of refraction} \end{array}$$

Next, match all the BCs at interface, namely:

$$\vec{D} \cdot \hat{n} \text{ and } \vec{B} \cdot \hat{n} \text{ continuous,}$$

$$\text{and } \vec{E} \times \hat{n} \text{ and } \vec{H} \times \hat{n} \text{ continuous}$$

(since no free surface charges or surface currents are assumed present)

Therefore, we see that:

$$\left(\epsilon (\vec{E}_{oi} + \vec{E}_{or}) - \epsilon' \vec{E}_{ot} \right) \cdot \hat{n} = 0$$

$$\left(\frac{n}{c} \hat{k}_i \times \vec{E}_{oi} + \frac{n}{c} \hat{k}_r \times \vec{E}_{or} - \frac{n'}{c} \hat{k}_t \times \vec{E}_{ot} \right) \cdot \hat{n} = 0$$

$$\left(\vec{E}_{oi} + \vec{E}_{or} - \vec{E}_{ot} \right) \times \hat{n} = 0$$

$$\left(\frac{1}{\mu} \frac{n}{c} \hat{k}_i \times \vec{E}_{oi} + \frac{1}{\mu} \frac{n}{c} \hat{k}_r \times \vec{E}_{or} - \frac{1}{\mu'} \frac{n'}{c} \hat{k}_t \times \vec{E}_{ot} \right) \times \hat{n} = 0$$

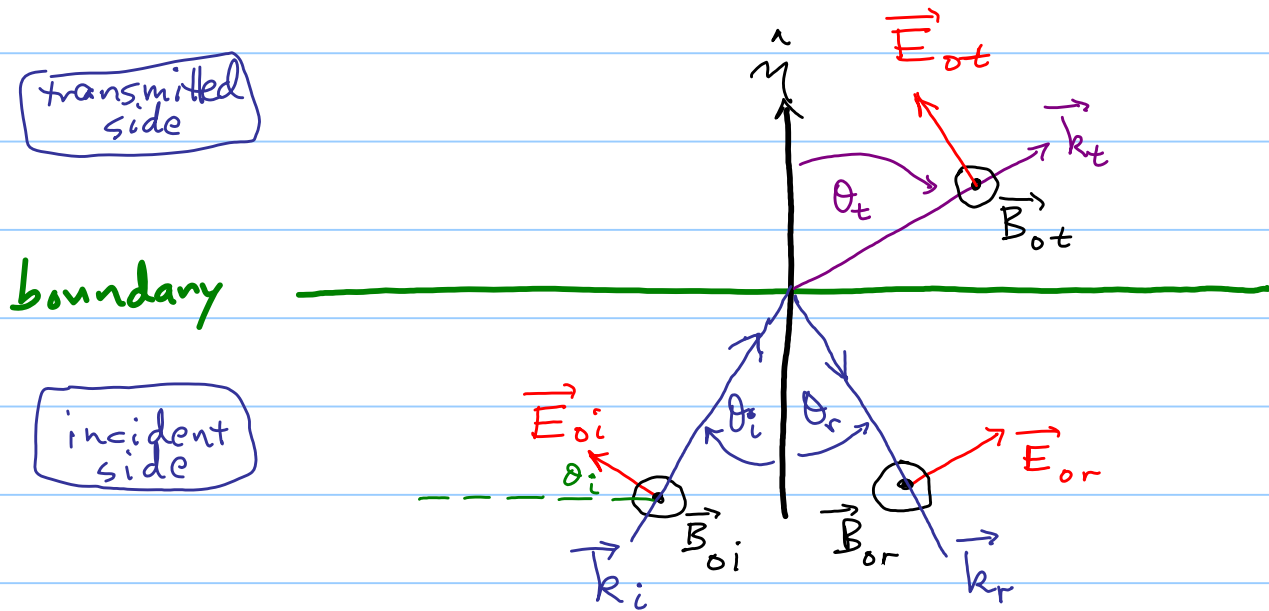
To apply these BCs, it is simplest to consider 2 separate cases:

(i) The incident linearly-polarized wave has $\vec{E}_{oi} \underline{\underline{\text{IN}}}$ the plane of incidence

(ii) The incident linearly-pol. wave has $\vec{E}_{oi}$ PERPENDICULAR to the plane of incidence

Of course, if the incident light has general elliptical polarization, it will just be a linear combination of these 2 cases.

Case (i) $\vec{E}_{oi}$ lies IN the plane of incidence "POI"



Now $\vec{D} \cdot \hat{n} = \text{continuous} \Rightarrow \epsilon E_{oi} \sin \theta_i + \epsilon E_{or} \sin \theta_r = \epsilon' E_{ot} \sin \theta_t$

and $\vec{E} \times \hat{n} = \text{continuous},$

$\Rightarrow E_{oi} \cos \theta_i - E_{or} \cos \theta_r = E_{ot} \cos \theta_t$

$E_{ot} \frac{\epsilon' n \sin \theta_i}{n'}$

and $\vec{H} \times \hat{n} = \text{continuous} \Rightarrow \frac{1}{\mu} (B_{oi} + B_{or}) = \frac{1}{\mu'} B_{ot}$

$\Rightarrow \frac{n}{\mu} (E_{oi} + E_{or}) = \frac{n'}{\mu'} E_{ot}$

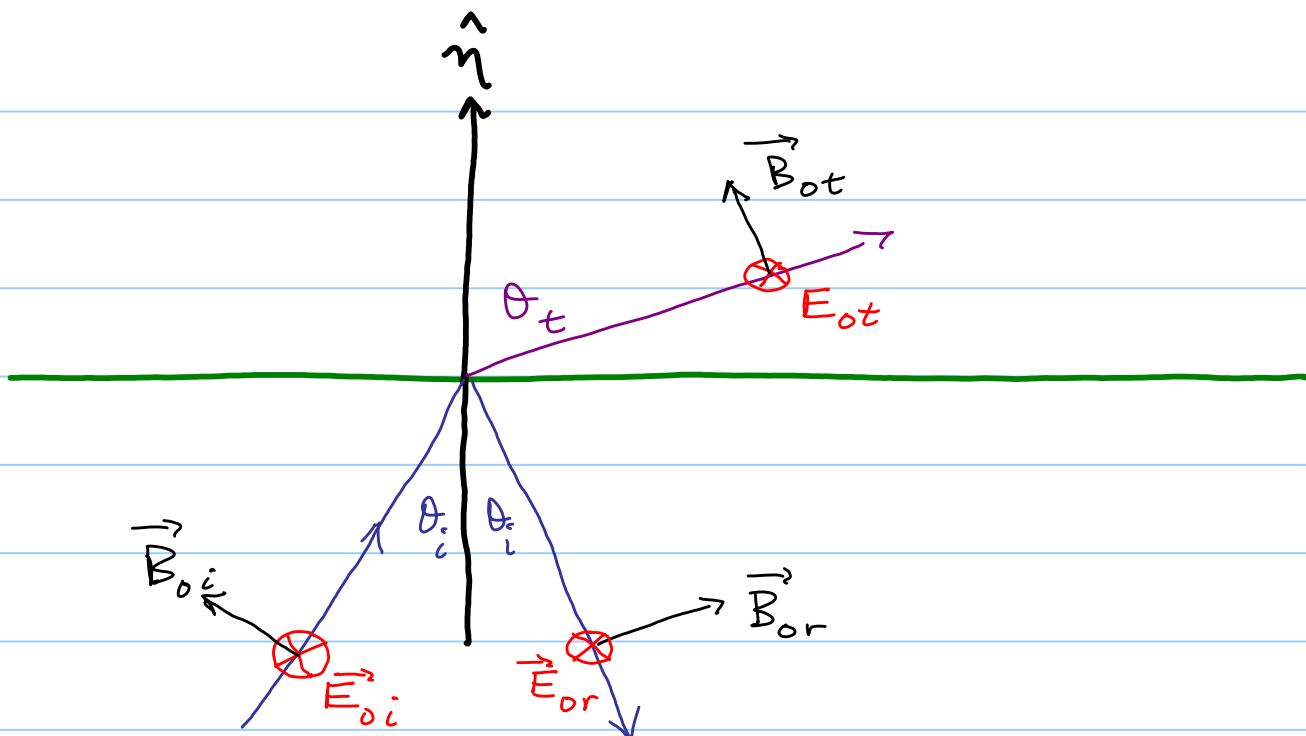
solution of these 2 equations, 2 unknowns, for an assumed known E_{oi} , gives:

$E_{or} = E_{oi} \frac{n' \mu \cos \theta_i - n \mu' \cos \theta_t}{n' \mu \cos \theta_i + n \mu' \cos \theta_t}$

for $\vec{E}_{oi} \perp \text{plane of incidence}$

$E_{ot} = E_{oi} \frac{2n \mu' \cos \theta_i}{n' \mu \cos \theta_i + n \mu' \cos \theta_t}$

Case (ii) $\vec{E}_{oi} \perp$ to P.O.I.



Continuity of $\vec{E} \times \hat{n} \Rightarrow E_{oi} + E_{or} = E_{ot}$

Continuity of $\vec{H} \times \hat{n} \Rightarrow \frac{1}{\mu} (B_{oi} \cos \theta_i - B_{or} \cos \theta_i) = \frac{B_{ot}}{\mu'} \cos \theta_t$

or $\frac{n}{\mu} (E_{oi} - E_{or}) \cos \theta_i = \frac{n'}{\mu'} E_{ot} \cos \theta_t$

Solution is:

$$E_{or} = E_{oi} \frac{n\mu' \cos \theta_i - n'\mu \cos \theta_t}{n\mu' \cos \theta_i + n'\mu \cos \theta_t}$$

$$E_{ot} = E_{oi} \frac{2n\mu' \cos \theta_i}{n\mu' \cos \theta_i + n'\mu \cos \theta_t}$$

$\vec{E}_{oi} \perp$
to P.O.I.

and we could eliminate θ_t using Snell's law,
if desired: $\cos \theta_t = \sqrt{1 - \frac{n^2}{n'^2} \sin^2 \theta_i}$

Specialized cases For optical frequencies it is usually accurate to set $\frac{\mu'}{\mu} \approx 1$, and this gives a simple result for the case of normal incidence, i.e. $\theta_i = 0$:

$$\underline{\vec{E}_{oi} \parallel \text{to P.O.I.}}$$

$$\frac{E_{or}}{E_{oi}} = \frac{n' - n}{n' + n}$$

$$\frac{E_{ot}}{E_{oi}} = \frac{2n}{n' + n}$$

$$\underline{\vec{E}_{oi} \perp \text{to P.O.I.}}$$

$$\frac{E_{or}}{E_{oi}} = \frac{n - n'}{n + n'}$$

$$\frac{E_{ot}}{E_{oi}} = \frac{2n}{n' + n}$$

These results for E_{or} appear to have a sign difference, a consequence of our choices of coordinate axes — not an actual difference!

Brewster's Angle — At a certain incidence angle θ_B , there is no reflected wave for the $\vec{E}$ -field component $\parallel$ to the P.O.I.

To work out the value of θ_B , just set $E_{or} = 0$ above, i.e. (again take $\frac{\mu'}{\mu} \approx 1$)

$$\frac{E_{or}}{E_{oi}} \propto \frac{\frac{n'}{n} \cos \theta_i - \sqrt{1 - \frac{n^2}{n'^2} \sin^2 \theta_i}}{(\text{denominator})} \xrightarrow{\theta_i \rightarrow \theta_B} 0$$

and we can solve for θ_B ,

$$\begin{aligned}\left(\frac{n'}{n}\right)^2 \cos^2 \theta_B &= 1 - \frac{n^2}{n'^2} \sin^2 \theta_B \\ &= \cos^2 \theta_B + \sin^2 \theta_B \left(1 - \frac{n^2}{n'^2}\right)\end{aligned}$$

$$\Rightarrow \tan^2 \theta_B = \frac{\left(\frac{n'}{n}\right)^2 - 1}{1 - \frac{n^2}{n'^2}} \quad \text{which simplifies to:}$$

$\tan \theta_B = \frac{n'}{n}$

 = Brewster angle

$\Rightarrow$ At the Brewster angle, all reflected light is polarized $\perp$ to the P.O.I., i.e. $\parallel$ to the surface itself.

e.g. - for a water surface,
 $\frac{n'}{n} \approx 1.35 \Rightarrow \theta_B(\text{water}) \approx 53^\circ$

while for glass, $\frac{n'}{n} \approx 1.5 \Rightarrow \theta_B(\text{glass}) \approx 56^\circ$

Next: Total internal reflection

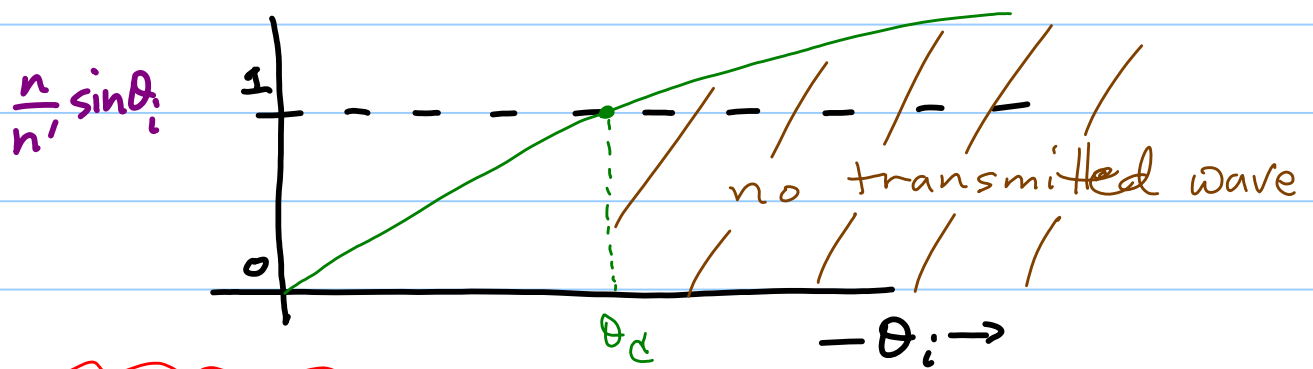
$\Rightarrow$ Suppose light is incident from a medium of higher refractive index, $n > n'$

e.g. water $\rightarrow$ air

Then since $\sin \theta_t = \frac{n}{n'} \sin \theta_i$,

or $\theta_t = \sin^{-1}\left(\frac{n}{n'} \sin \theta_i\right)$

$\Rightarrow$ beyond a certain angle $\theta_i > \theta_c$, clearly $\frac{n}{n'} \sin \theta_i > 1$ so it has no real arcsin,



$$\Rightarrow \theta_c = \sin^{-1}\left(\frac{n'}{n}\right) \equiv \text{critical angle}$$

$\Rightarrow$ no transmitted light and the reflection is total

We can explore the nature of the transmitted wave at $\theta_i > \theta_c$, by analytically continuing our previous derived solution, which simply means inserting $k_t \rightarrow \text{imaginary}$!

To see this, recall that Snell's law was derived from $\vec{k}_i \cdot \vec{x} \Big|_{z=0} = \vec{k}_t \cdot \vec{x} \Big|_{z=0}$

$$\Rightarrow k_i \sin \theta_i = k_t \sin \theta_t$$

$$\text{or } \frac{n\omega}{c} \sin \theta_i = \frac{n'\omega}{c} \sin \theta_t$$

i.e. the component of $\vec{k}^2 \parallel$ to interface is continuous, $\Rightarrow k_{ix} = k_{tx}$

So when $\frac{n}{n'} \sin \theta_i > 1$, for $\theta_i > \theta_c$,

$$\Rightarrow \sin \theta_t > 1, \text{ whereby } \cos^2 \theta_t = 1 - \sin^2 \theta_t < 0$$

$$\Rightarrow \cos \theta_t = \text{purely imaginary}$$

But the normal component of the transmitted wave vector $\vec{k}_t$ is $k_{tz} = k_t \cos \theta_t \rightarrow \text{imaginary}$
 $\equiv iK$

$$\text{where } K = \sqrt{\frac{n^2}{n'^2} \sin^2 \theta_i - 1}$$

Then the transmitted wave looks like

$$\vec{E}_t = \vec{E}_{ot} e^{i\vec{k}_t \cdot \vec{r}} = \vec{E}_{ot} e^{i(k_{tz}z + k_{tx}x)}$$

$$\Rightarrow \vec{E}_t = \vec{E}_{ot} e^{-Kz} e^{ik_t \sin \theta x}$$

and we note this exponential damping of the transmitted wave in the direction normal to the surface.

Let's calculate the time-averaged energy flow through the surface:

$$\langle \vec{S} \cdot \hat{z} \rangle = \frac{1}{2} \text{Re} \left(\hat{z} \cdot \vec{E}_t \times \vec{H}^* \right)$$

$$\begin{aligned} \text{where } \vec{H}_t &= (\mu' \epsilon')^{1/2} \hat{k}_t \times \vec{E}_t = \frac{c}{n' \omega} \left(\frac{\mu' \epsilon'}{\mu'} \right)^{1/2} \vec{k}_t \times \vec{E}_t \\ &= \frac{1}{\mu' \omega} \vec{k}_t \times \vec{E}_t \end{aligned}$$

$$\begin{aligned}
 \text{Thus } \langle \vec{S} \cdot \hat{z} \rangle &= \frac{1}{2} \operatorname{Re} \left[\hat{z} \cdot \vec{E}_t \times (\vec{k}_t \times \vec{E}_t)^* \right] \frac{1}{\mu' \omega} \\
 &= \frac{1}{2\mu' \omega} \operatorname{Re} (\hat{z} \cdot \vec{k}_t |\vec{E}_t|^2) \\
 &= 0 \quad \text{since } \operatorname{Re}(k_{tz}) = 0 !
 \end{aligned}$$

$\Rightarrow$ ALL ENERGY is reflected!

On your own, read about:

- Evanescent waves
- light tunneling across a total internal reflection gap

