

Physics 42200

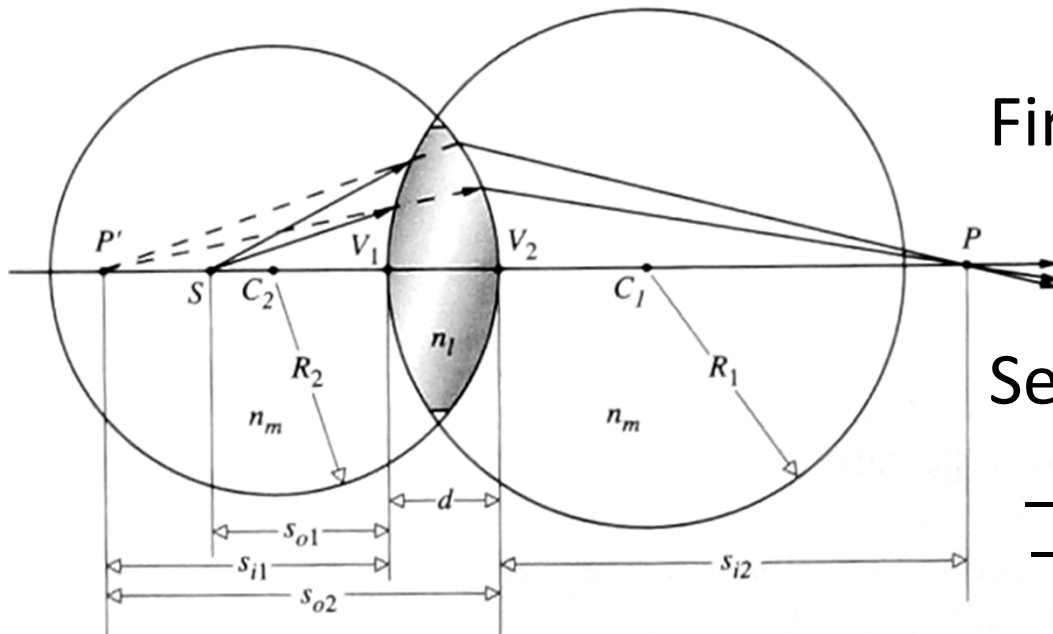
# Waves & Oscillations

Lecture 27 – Geometric Optics

Spring 2014 Semester

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# Thin Lens Equation



First surface:

$$\frac{n_m}{s_{o1}} + \frac{n_l}{s_{i1}} = \frac{n_l - n_m}{R_1}$$

Second surface:

$$\frac{n_l}{-s_{i1} + d} + \frac{n_m}{s_{i2}} = \frac{n_m - n_l}{R_2}$$

Add these equations and simplify using  $n_m = 1$  and  $d \rightarrow 0$ :

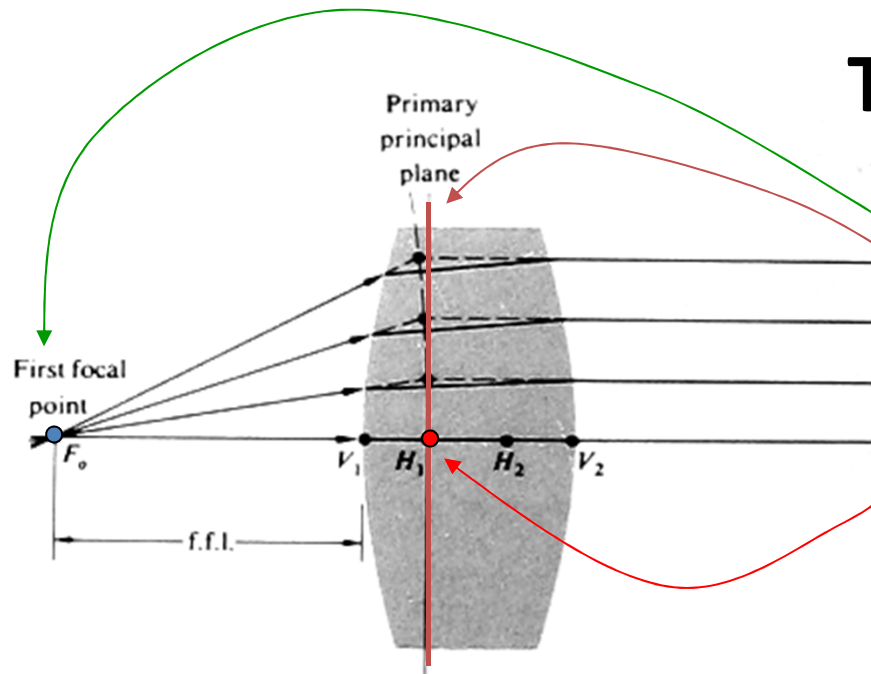
$$\frac{1}{s_o} + \frac{1}{s_i} = (n_l - 1) \left( \frac{1}{R_1} - \frac{1}{R_2} \right)$$

(Thin lens equation)

# Thick Lenses

- Eliminate the intermediate image distance,  $s_{i1}$
- Focal points:
  - Rays passing through the focal point are refracted parallel to the optical axis by both surfaces of the lens
  - Rays parallel to the optical axis are refracted through the focal point
  - For a thin lens, we can draw the point where refraction occurs in a common plane
  - For a thick lens, refraction for the two types of rays can occur at different planes

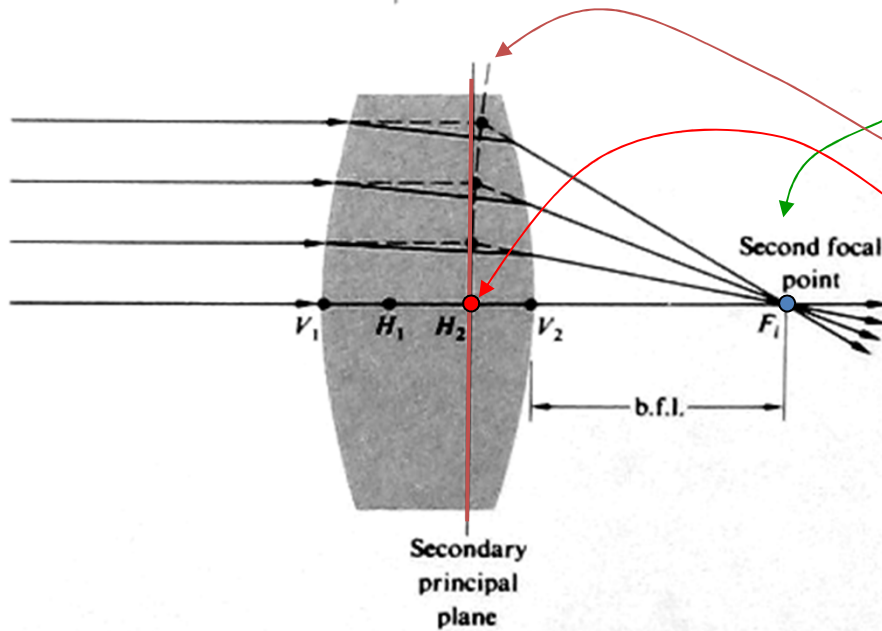
# Thick Lens: definitions



First focal point (front focal length)

Primary principal plane

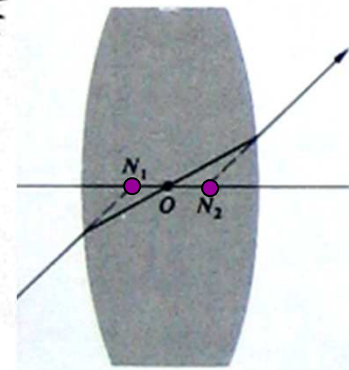
First principal point



Second focal point (back focal length)

Secondary principal plane

Second principal point



Nodal points

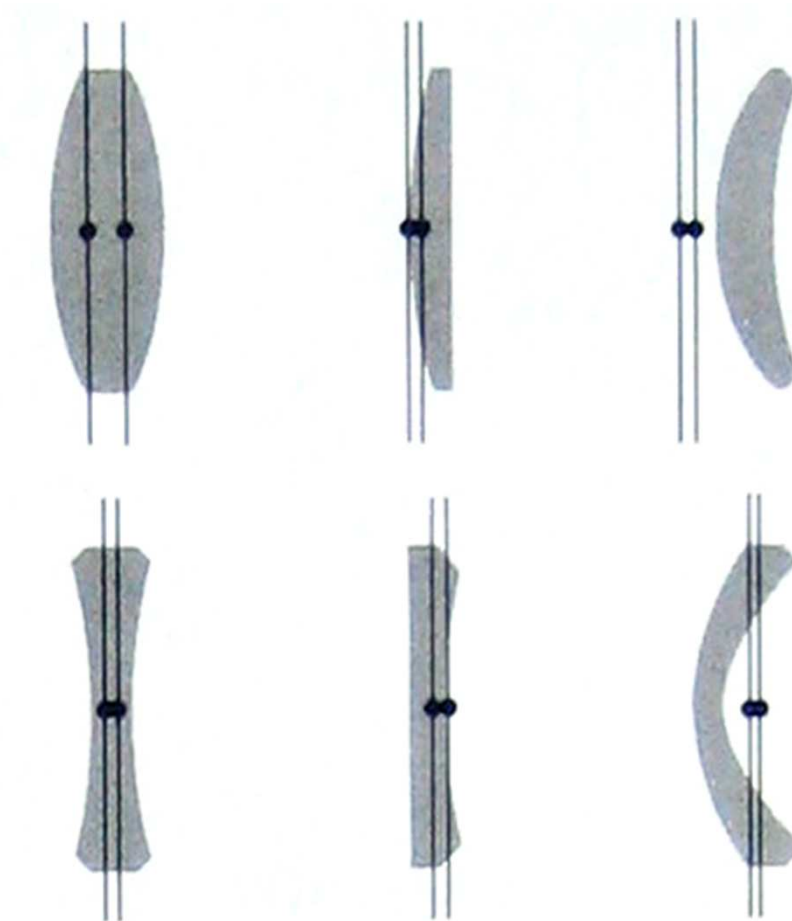
If media on both sides has the same  $n$ , then:

$$N_1 = H_1 \text{ and } N_2 = H_2$$

$F_o F_i H_1 H_2 N_1 N_2$  - cardinal points

# Thick Lens: Principal Planes

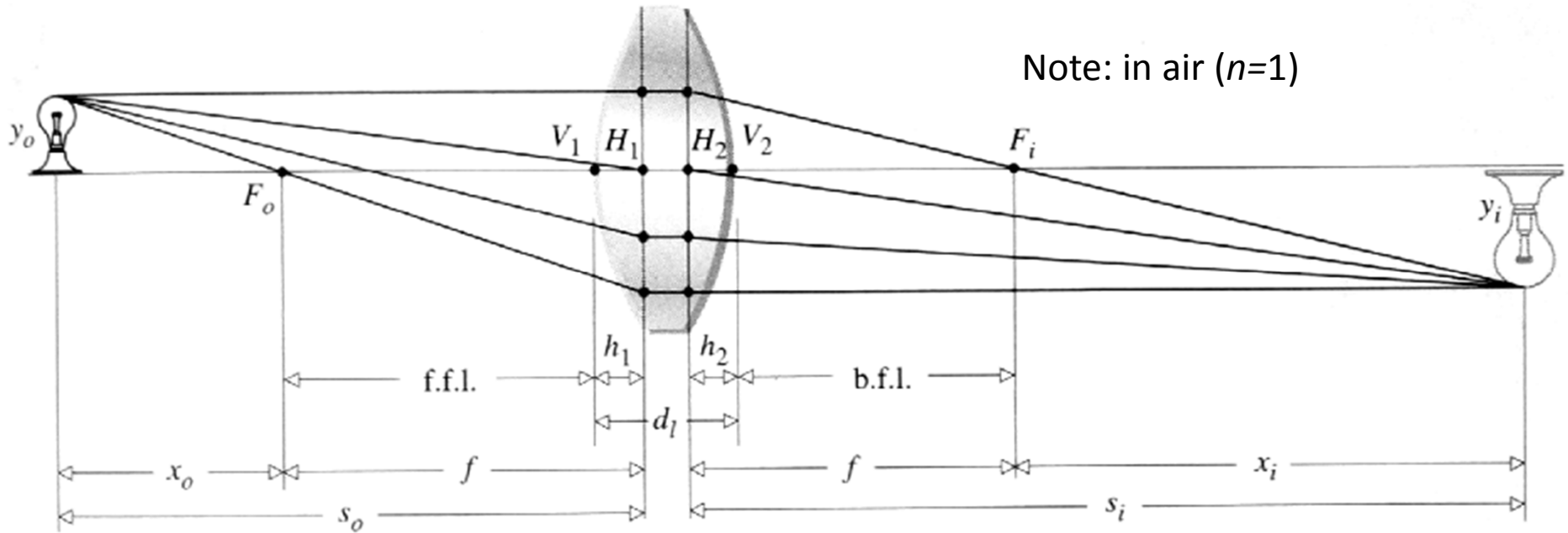
Principal planes can lie outside the lens:



# Thick Lenses and Principal Planes

- For a single refracting surface, we measured  $s_i$  and  $s_o$  with respect to the vertex (ie, the surface of the lens)
- For a thick lens, we need to define  $s_i$  and  $s_o$  with respect to the principal planes.
- We need to calculate where they are, but it makes the algebra simpler.
- We are not going to derive the following formula...

# Thick Lens: equations



$$\frac{1}{s_o} + \frac{1}{s_i} = \frac{1}{f}$$

$x_o x_i = f^2$  ← effective focal length:

$$\frac{1}{f} = (n_l - 1) \left[ \frac{1}{R_1} - \frac{1}{R_2} + \frac{(n_l - 1)d_l}{n_l R_1 R_2} \right]$$

Principal planes:

$$h_1 = -\frac{f(n_l - 1)d_l}{n_l R_2}$$

$$h_2 = -\frac{f(n_l - 1)d_l}{n_l R_1}$$

Magnification:

$$M_T \equiv \frac{y_i}{y_o} = -\frac{s_i}{s_o} = -\frac{x_i}{f} = -\frac{f}{x_o}$$

# Thick Lens Calculations

1. Calculate focal length

$$\frac{1}{f} = (n - 1) \left[ \frac{1}{R_1} - \frac{1}{R_2} + \frac{(n - 1)d}{nR_1R_2} \right]$$

2. Calculate positions of principal planes

$$h_1 = -\frac{f(n - 1)d}{nR_2}$$
$$h_2 = -\frac{f(n - 1)d}{nR_1}$$

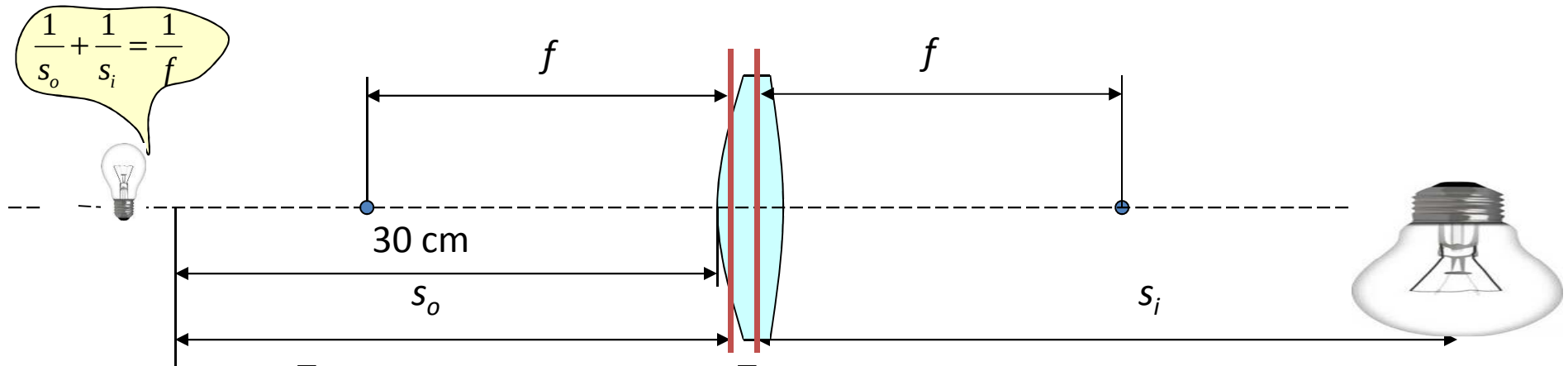
3. Calculate object distance,  $s_o$ , measured from principal plane
4. Calculate image distance:

$$\frac{1}{s_o} + \frac{1}{s_i} = \frac{1}{f}$$

5. Calculate magnification,  $m_T = -s_i/s_o$

# Thick Lens: example

Find the image distance for an object positioned 30 cm from the vertex of a double convex lens having radii 20 cm and 40 cm, a thickness of 1 cm and  $n_l=1.5$



$$\frac{1}{f} = (n_l - 1) \left[ \frac{1}{R_1} - \frac{1}{R_2} + \frac{(n_l - 1)d_l}{n_l R_1 R_2} \right] = 0.5 \left[ \frac{1}{20} - \frac{1}{-40} + \frac{0.5 \cdot 1}{1.5 \cdot 20 \cdot 40} \right] \frac{1}{\text{cm}}$$

$$f = 26.8 \text{ cm}$$

$$h_1 = -\frac{26.8 \cdot 0.5 \cdot 1}{-40 \cdot 1.5} \text{ cm} = 0.22 \text{ cm}$$

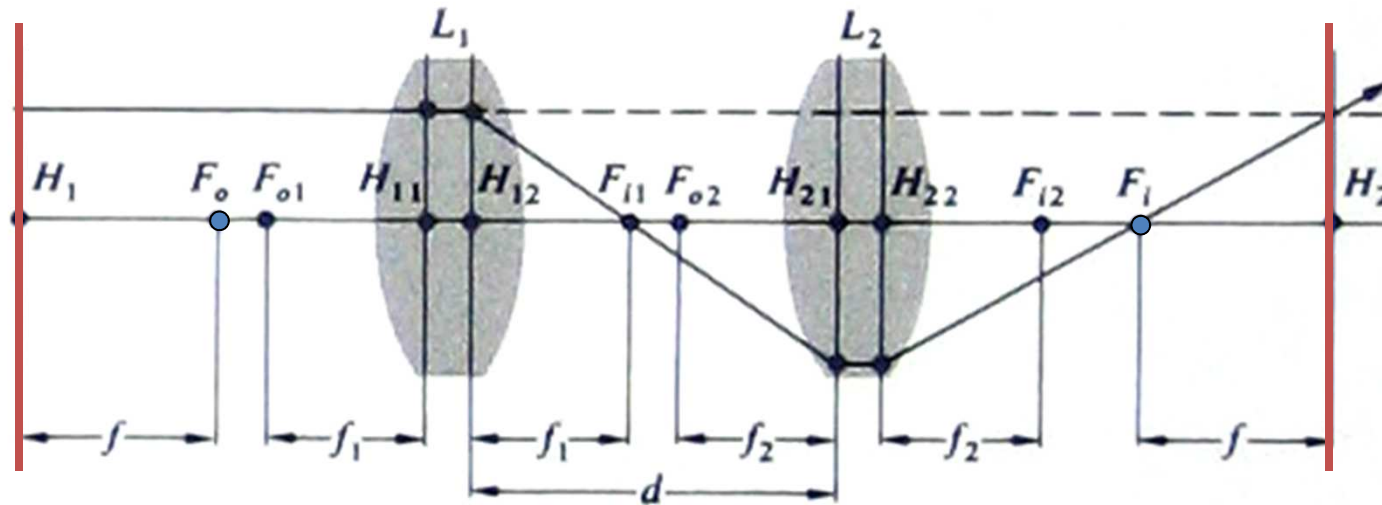
$$h_2 = -\frac{26.8 \cdot 0.5 \cdot 1}{20 \cdot 1.5} \text{ cm} = -0.44 \text{ cm}$$

$$s_o = 30 \text{ cm} + 0.22 \text{ cm} = 30.22 \text{ cm}$$

$$\frac{1}{30.22 \text{ cm}} + \frac{1}{s_i} = \frac{1}{26.8 \text{ cm}}$$

$$s_i = 238 \text{ cm}$$

# Compound Thick Lens



Can use two principal points (planes) and effective focal length  $f$  to describe propagation of rays through any compound system

*Note:* any ray passing through the first principal plane will emerge at the same height at the second principal plane

For 2 lenses (above):

$$\frac{1}{f} = \frac{1}{f_1} + \frac{1}{f_2} - \frac{d}{f_1 f_2}$$

$$\overline{H_{11}H_1} = fd / f_2$$

$$\overline{H_{22}H_2} = fd / f_1$$

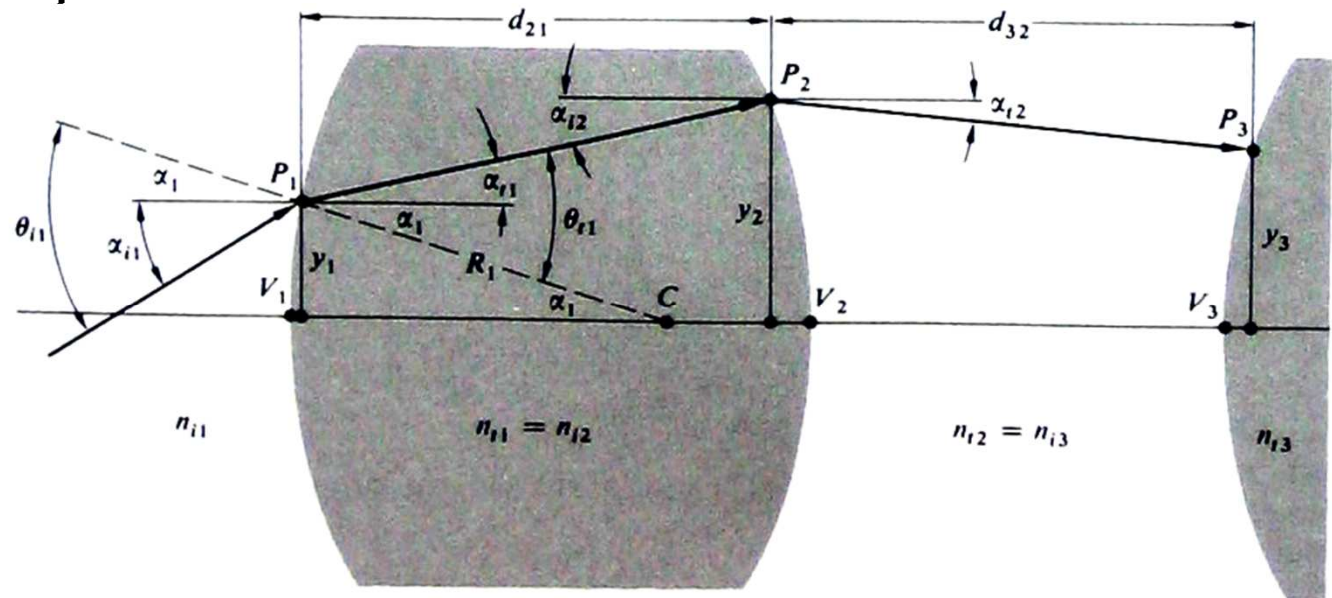
Example: page 246

# Ray Tracing

- Even the thick lens equation makes approximations and assumptions
  - Spherical lens surfaces
  - Paraxial approximation
  - Alignment with optical axis
- The only physical concepts we applied were
  - Snell's law:  $n_i \sin \theta_i = n_t \sin \theta_t$
  - Law of reflection:  $\theta_t = \theta_i$  (in the case of mirrors)
- Can we do better? Can we solve for the paths of the rays exactly?
  - Sure, no problem! But it is a lot of work.
  - Computers are good at doing lots of work (without complaining)

# Ray Tracing

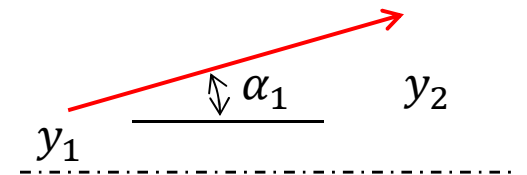
- We will still make the assumptions of
  - Paraxial rays
  - Lenses aligned along optical axis
- We will make no assumptions about the lens thickness or positions.
- Geometry:



# Ray Tracing

- At a given point along the optical axis, each ray can be uniquely represented by two numbers:
  - Distance from optical axis,  $y_i$
  - Angle with respect to optical axis,  $\alpha_i$
- If the ray does not encounter an optical element its distance from the optical axis changes according to the *transfer equation*:

$$y_2 = y_1 + d_1 \alpha_1$$



- This assumes the paraxial approximation  $\sin \alpha_1 \approx \alpha_1$

# Ray Tracing

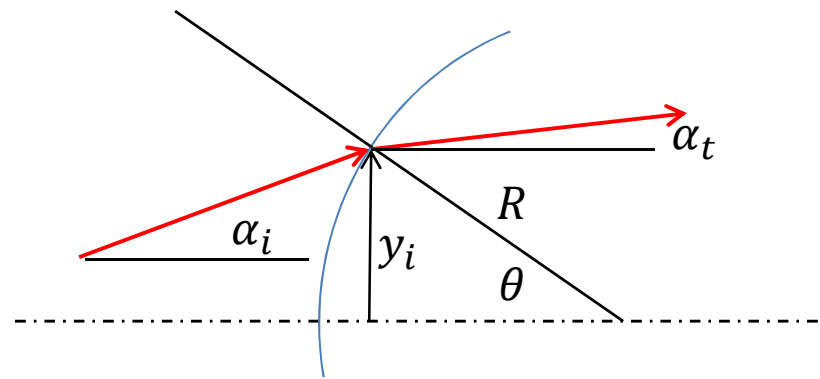
- At a given point along the optical axis, each ray can be uniquely represented by two numbers:
  - Distance from optical axis,  $y_i$
  - Angle with respect to optical axis,  $\alpha_i$
- When the ray encounters a surface of a material with a different index of refraction, its angle will change according to the *refraction equation*:

$$n_{t1}\alpha_{t1} = n_{i1}\alpha_{i1} - D_1y_1$$
$$D_1 = \frac{n_{t1} - n_{i1}}{R_1}$$

- Also assumes the paraxial approximation

# Ray Tracing

- Geometry used for the refraction equation:



$$\sin \theta = \frac{y_i}{R} \approx \theta$$

$$\theta_i = \alpha_i + \theta = \alpha_i + y_i/R$$

$$\theta_t = \alpha_t + \theta = \alpha_t + y_i/R$$

$$n_i \theta_i = n_t \theta_t$$

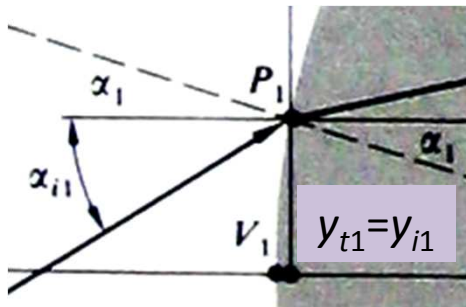
$$n_i \alpha_i + \frac{n_i y_i}{R} = n_t \alpha_t + \frac{n_t y_i}{R}$$

$$n_t \alpha_t = n_i \alpha_i - \left( \frac{n_t - n_i}{R} \right) y_i$$

# Matrix Treatment: Refraction

At any point of space need 2 parameters to fully specify ray: distance from axis ( $y$ ) and inclination angle ( $\alpha$ ) with respect to the optical axis. Optical element changes these ray parameters.

Refraction:



$$n_{t1}\alpha_{t1} = n_{i1}\alpha_{i1} - D_1 y_{i1}$$

$$y_{t1} = 0 \cdot n_{i1}\alpha_{i1} + y_{i1}$$

*note: paraxial approximation*

Reminder:

$$\begin{pmatrix} A & B \\ C & D \end{pmatrix} \begin{pmatrix} \alpha \\ y \end{pmatrix} \equiv \begin{pmatrix} A\alpha + By \\ C\alpha + Dy \end{pmatrix}$$

Equivalent matrix representation:

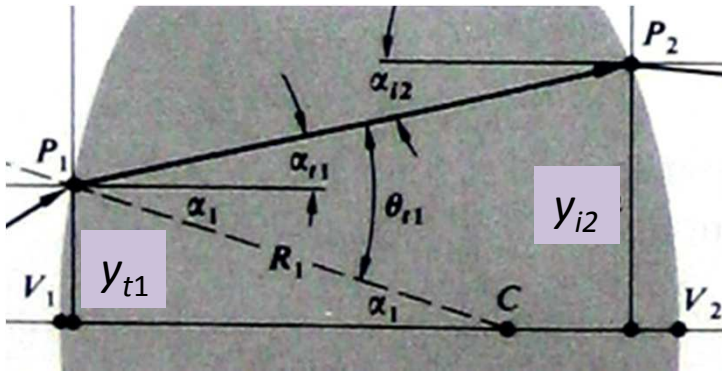
$$\begin{pmatrix} n_{t1}\alpha_{t1} \\ y_{t1} \end{pmatrix} = \begin{pmatrix} 1 & -D_1 \\ 0 & 1 \end{pmatrix} \begin{pmatrix} n_{i1}\alpha_{i1} \\ y_{i1} \end{pmatrix}$$

$$\mathbf{r}_{t1} = \mathbf{R}_1 \mathbf{r}_{i1}$$

$\uparrow \equiv \mathbf{r}_{i1}$  - input ray  
 $\uparrow \equiv \mathbf{R}_1$  - **refraction matrix**  
 $\uparrow \equiv \mathbf{r}_{t1}$  - output ray

# Matrix: Transfer Through Space

Transfer:



$$n_{i2}\alpha_{i2} = n_{t1}\alpha_{t1} + 0 \cdot y_{t1}$$

$$y_{i2} = d_{21} \cdot \alpha_{t1} + y_{t1}$$

Equivalent matrix presentation:

$$\begin{pmatrix} n_{i2}\alpha_{i2} \\ y_{i2} \end{pmatrix} = \begin{pmatrix} 1 & 0 \\ d_{21}/n_{t1} & 1 \end{pmatrix} \begin{pmatrix} n_{t1}\alpha_{t1} \\ y_{t1} \end{pmatrix}$$

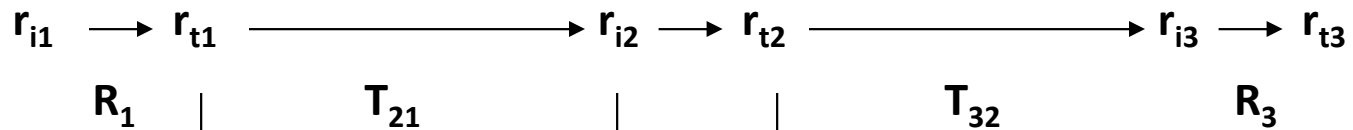
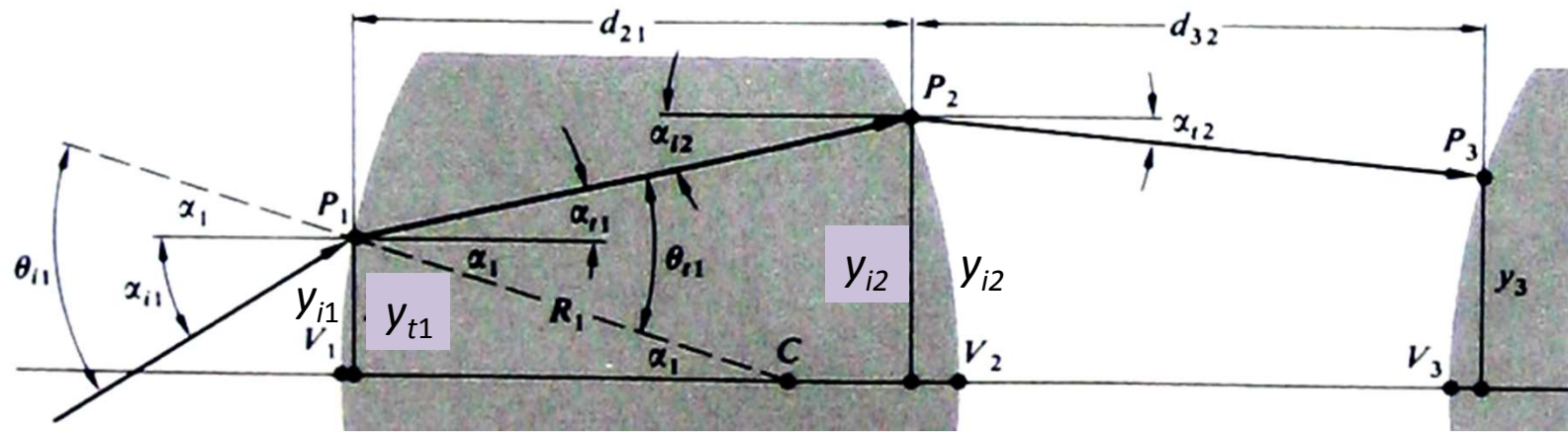
$$\mathbf{r}_{i2} = \mathbf{T}_{21} \mathbf{r}_{t1}$$

$\equiv \mathbf{r}_{i2}$  - output ray

$\equiv \mathbf{T}_{21}$  - *transfer matrix*

$\equiv \mathbf{r}_{t1}$  - input ray

# System Matrix



$$\mathbf{r}_{t1} = \mathbf{R}_1 \mathbf{r}_{i1}$$

$$\mathbf{r}_{i2} = \mathbf{T}_{21} \mathbf{r}_{t1} = \mathbf{T}_{21} \mathbf{R}_1 \mathbf{r}_{i1}$$

Thick lens ray transfer:

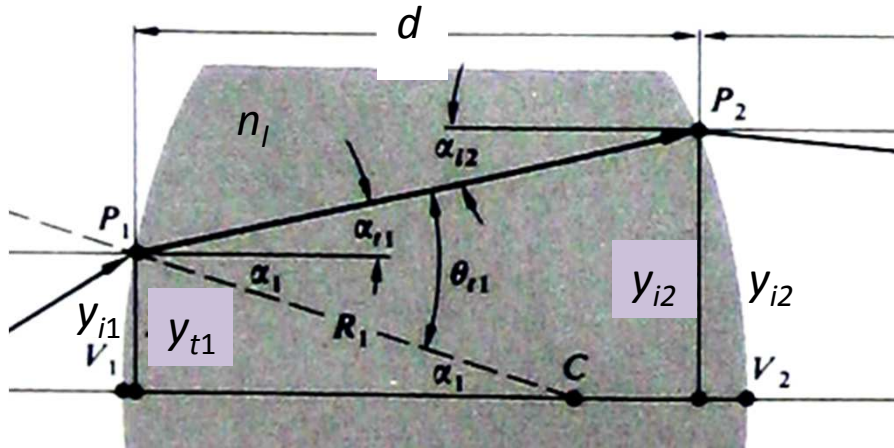
$$\mathbf{r}_{t2} = \mathbf{R}_2 \mathbf{T}_{21} \mathbf{R}_1 \mathbf{r}_{i1}$$

System matrix:

$$\mathbf{A} = \mathbf{R}_2 \mathbf{T}_{21} \mathbf{R}_1 \rightarrow \mathbf{r}_{t2} = \mathbf{A} \mathbf{r}_{i1}$$

Can treat any system with single system matrix

# Thick Lens Matrix



Reminder:

$$\begin{pmatrix} A & B \\ C & D \end{pmatrix} \begin{pmatrix} a & b \\ c & d \end{pmatrix} \equiv \begin{pmatrix} Aa + Bc & Ab + Bd \\ Ca + Dc & Cb + Dd \end{pmatrix}$$

$$\mathbf{A} = \begin{pmatrix} 1 & -D_2 \\ 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & 0 \\ d_l/n_l & 1 \end{pmatrix} \begin{pmatrix} 1 & -D_1 \\ 0 & 1 \end{pmatrix}$$

$$\mathbf{A} = \begin{pmatrix} 1 - \frac{D_2 d_l}{n_l} & -D_1 - D_2 + \frac{D_1 D_2 d_l}{n_l} \\ \frac{d_l}{n_l} & 1 - \frac{D_1 d_l}{n_l} \end{pmatrix}$$

$$\mathbf{A} = \mathbf{R}_2 \mathbf{T}_{21} \mathbf{R}_1$$

$$\mathbf{R} = \begin{pmatrix} 1 & -D \\ 0 & 1 \end{pmatrix}$$

$$\mathbf{T} = \begin{pmatrix} 1 & 0 \\ d/n & 1 \end{pmatrix}$$

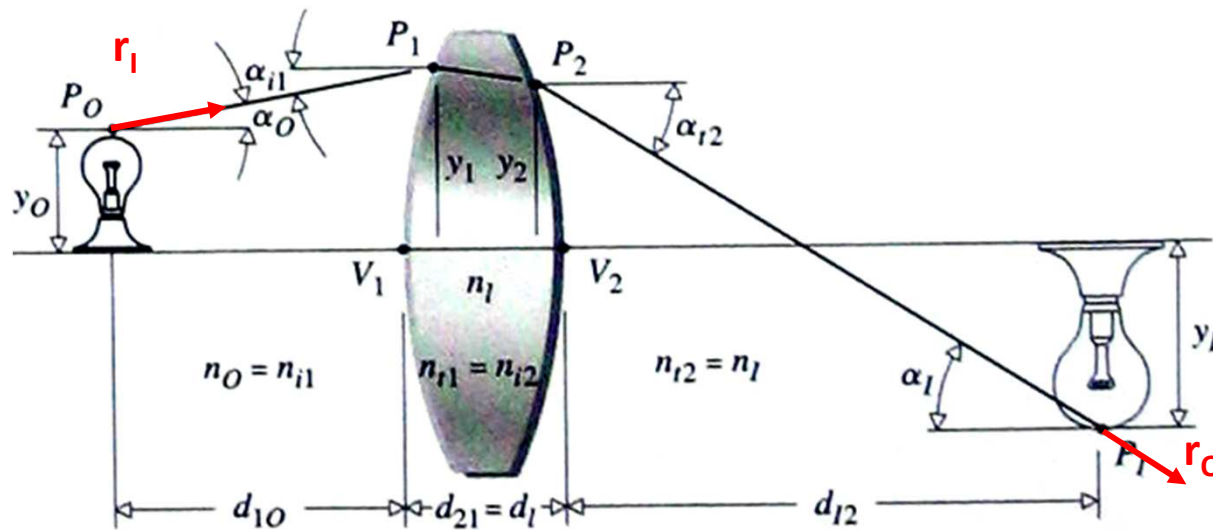
$$\frac{1}{f} = (n_l - 1) \left( \frac{1}{R_1} - \frac{1}{R_2} \right)$$

system matrix of thick lens

For thin lens  $d_l=0$

$$\mathbf{A} = \begin{pmatrix} 1 & -1/f \\ 0 & 1 \end{pmatrix}$$

# Matrix Treatment: example



$$\mathbf{r}_I = \mathbf{T}_1 \mathbf{A}_l \mathbf{T}_2 \mathbf{r}_O$$

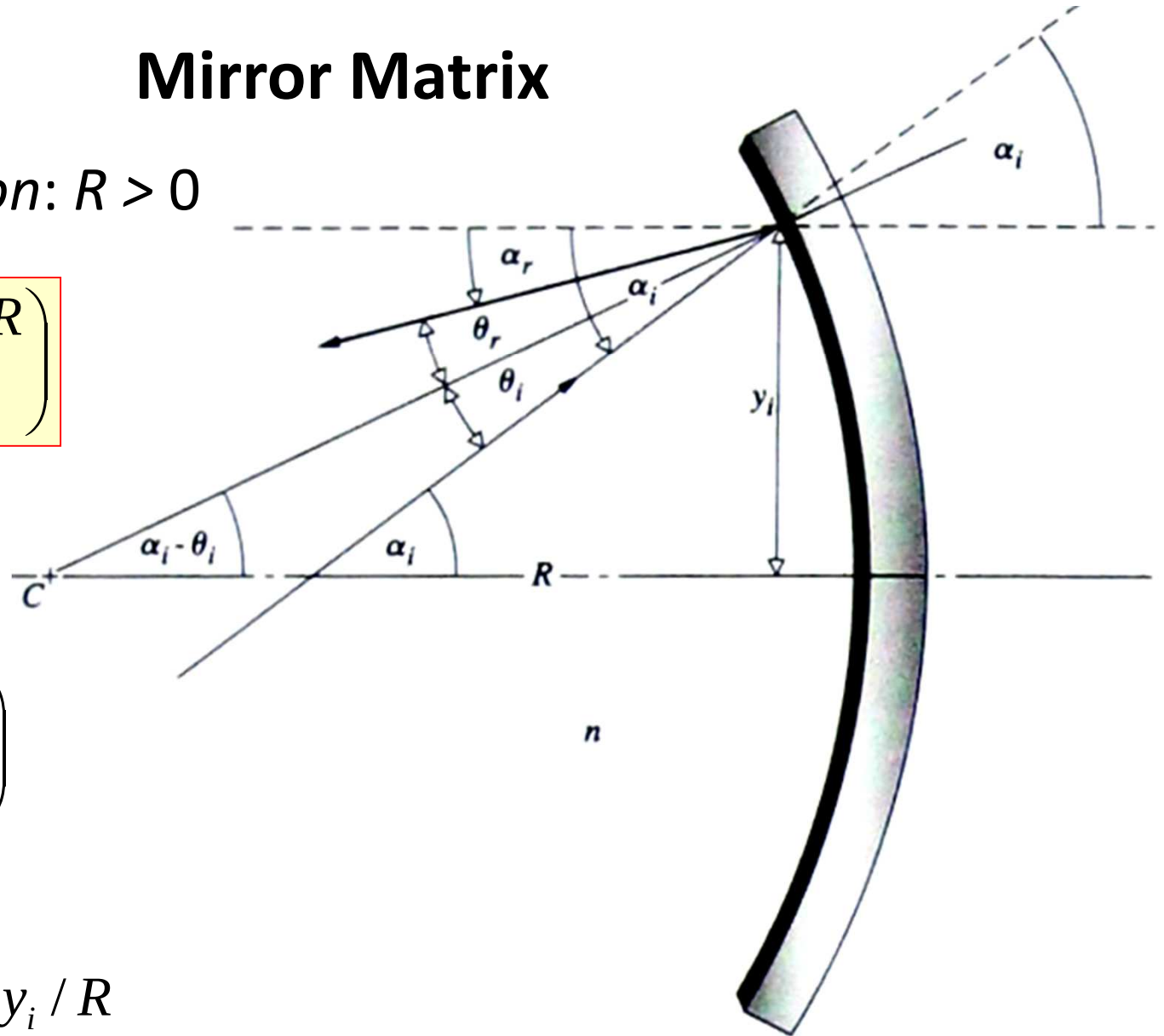
$$\begin{pmatrix} n_I \alpha_I \\ y_I \end{pmatrix} = \begin{pmatrix} 1 & 0 \\ d_{I2}/n_I & 1 \end{pmatrix} \begin{pmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{pmatrix} \begin{pmatrix} 1 & 0 \\ d_{10}/n_O & 1 \end{pmatrix} \begin{pmatrix} n_O \alpha_O \\ y_O \end{pmatrix}$$

(Detailed example with thick lenses and numbers: page 250)

# Mirror Matrix

Sign convention:  $R > 0$

$$\mathbf{M} = \begin{pmatrix} -1 & 2n/R \\ 0 & 1 \end{pmatrix}$$



$$\begin{pmatrix} n\alpha_r \\ y_r \end{pmatrix} = \mathbf{M} \begin{pmatrix} n\alpha_i \\ y_i \end{pmatrix}$$

$$y_r = y_i$$

$$n\alpha_r = -n\alpha_i + 2ny_i / R$$

$$\alpha_r = -\alpha_i + 2y_i / R$$