

Review of Magnetostatics

Stationary charges \Rightarrow electrostatics

Steady currents \Rightarrow magnetostatics

Electric
currents

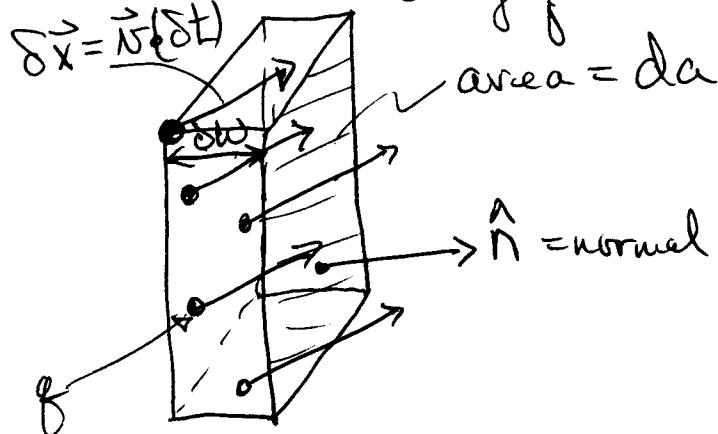
i) $I =$ rate charge is transported thru a

$$= \frac{dQ}{dt} = \frac{\text{given surface}}{\text{sec}} = \text{ampere}$$

ii) Current density (direction of positive charge flow)

Conducting medium $N = \frac{\# \text{ of charge carriers}}{\text{vol.}}$

each have charge q



$$d\vec{s} = \hat{n} da$$

$\vec{v}_d = \text{drift velocity}$

$$\text{Volume} = \Delta x \Delta y \Delta z = \hat{n} \cdot \vec{v}_d \cdot da \Delta t$$

$\delta Q =$ charge pass thru da in Δt

$$= (qN)(\text{volume}) = qN \vec{v}_d \cdot \hat{n} da \Delta t$$

$$= qN \vec{v}_d \cdot d\vec{s} \Delta t$$

$$\text{Current flowing thru } da \quad dI = \frac{\delta Q}{\Delta t} = N q \vec{v}_d \cdot d\vec{s}$$

$$= \int \vec{J} \cdot d\vec{s}$$

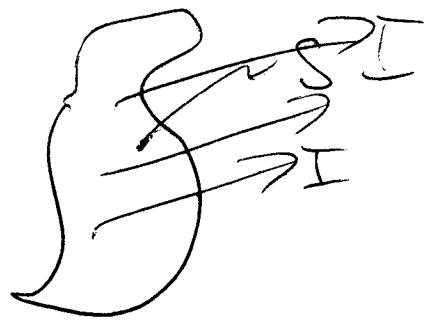
$$\vec{J} = N \vec{g} \vec{\nu} = \sum_i N_i g_i \vec{\nu}_i =$$

= current density
 = current / area
 = flux rate of charge flow

$$dI = \vec{J} \cdot d\vec{S}$$

Current thru arb. surface

$$I = \int_S \vec{J} \cdot d\vec{S}$$



I.3.) Continuity equation

$\partial V = S$

$$\vec{J} \cdot \hat{n} da = I$$

by Gauss's Thm.

$$= + \int_S \vec{J} \cdot \hat{n} da$$

$$= + \int_V \nabla \cdot \vec{J} dV$$

\vec{J} flows out $\frac{dQ}{dt}$ in volume

Q decreases $\frac{dQ}{dt}$

$$Q(t) = \int_V \rho(r, t) dV$$

$$= - \int_V \frac{\partial \rho}{\partial t} dV$$

Vis arb.

$$\Rightarrow \boxed{\frac{\partial \rho}{\partial t} + \nabla \cdot \vec{J} = 0}$$

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I.4) In general \vec{E} causes charges to drift $\Rightarrow \vec{J}$

For Ohmic (linear) material

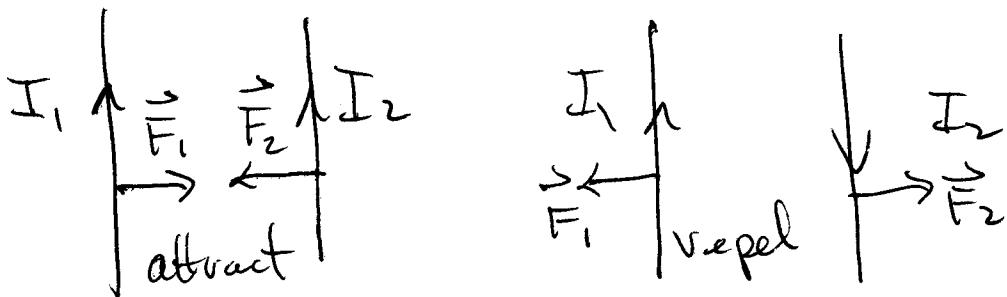
$$\vec{J} = g \vec{E} \quad \text{conductivity}$$

$$\Rightarrow \Delta\varphi = IR, \quad R = \frac{gA}{l} \quad \text{Ohm's law}$$

$$P = I^2 R = \frac{(I\Delta\varphi)^2}{R} = I\Delta\varphi.$$

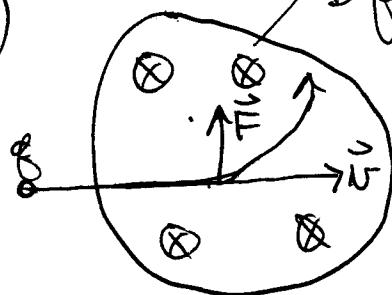
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II) Lorentz Force Law



1) Experiment $F_i \propto I_i \propto qN$ of charge in wire

2) \vec{B} field into paper



$$q\text{-moves } \perp \text{ to } \vec{v} \text{ & } \vec{B} \\ \Rightarrow \vec{F} \propto q \vec{v} \times \vec{B}$$

choose units of \vec{B} so that

$$\vec{F} = q \vec{v} \times \vec{B} ; \text{ add } \vec{E}$$

$$\boxed{\vec{F} = q(\vec{E} + \vec{v} \times \vec{B})}$$

$$\text{unit } B = \frac{\text{mass}}{\text{charge time}} = \text{Tesla}$$

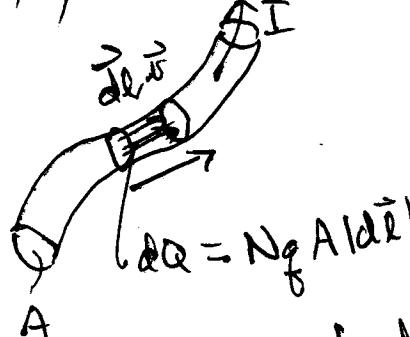
$$(1 \text{ Tesla})(1 \text{ coul})(\frac{1 \text{ m}}{\text{sec}}) = (\text{newton})$$

$$10^{-4} \text{ T} = 1 \text{ Gauss}$$

Earth's B field $\sim 3-6 \text{ G}$

Electromagnets $\sim 2 \text{ T} \sim 100 \text{ T}$
nuclei $\sim 10^4 \text{ T}$

II. 3) Currents interact with known \vec{B} -field



$$\begin{aligned} d\vec{F} &= dQ \vec{N} \times \vec{B} \\ &= NA_g |d\vec{l}| \vec{N} \times \vec{B} \quad \text{but } d\vec{l} \parallel \vec{N} \\ &= NA_g (\vec{\omega}) |d\vec{l}| \vec{N} \times \vec{B} \\ \text{but } I &= NA_g (\vec{\omega}) \end{aligned}$$

So

$$\boxed{d\vec{F} = I d\vec{l} \times \vec{B}}$$

If \vec{B} uniform: $\vec{F} = \oint_C d\vec{F} = 0$ for closed circuit

4) Torque $d\vec{\tau} = \vec{r} \times d\vec{F}$
 $= I \vec{r} \times (d\vec{l} \times \vec{B})$

$$\vec{\tau} = I \oint_C \vec{r} \times (d\vec{l} \times \vec{B})$$

If \vec{B} is uniform: $\vec{\tau} = I \vec{A} \times \vec{B} = \vec{\mu} \times \vec{B}$

$$\vec{A} = \iint_S d\vec{S} = \frac{1}{2} \oint_C \vec{r} \times d\vec{r} \quad \begin{matrix} \leftarrow \text{magnetic} \\ \text{dipole moment} \end{matrix}$$

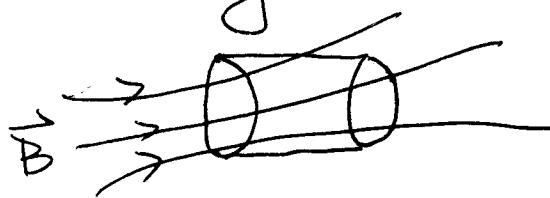
5) Current density $J = \vec{J} \cdot d\vec{S}$ So

$$\begin{aligned} I d\vec{l} &= \vec{J} \cdot d\vec{S} d\vec{l} \quad \text{but } \vec{J} \parallel d\vec{l} \Rightarrow \\ &= \vec{J} d\vec{S} \cdot d\vec{l} = \vec{J} dV \end{aligned}$$

$$\text{e.g. } d\vec{m} = \frac{1}{2} \vec{r} \times \vec{J} dV.$$

III.) No Magnetic Charge:

Experimentally \vec{B} lines are continuous
never a source or sink \Rightarrow flux of \vec{B}
through any closed surface = 0



Same # of lines enter
as leave volume

$$\oint \vec{B} \cdot d\vec{S} = 0$$

s || Gauss's law.

$$\int \vec{\nabla} \cdot \vec{B} dV, \text{ Varbi} \Rightarrow \boxed{\vec{\nabla} \cdot \vec{B} = 0}$$

Fundamental law
of magnetism
no mag. monopoles.

IV) Biot - Savart Law (1820) Ampere experimental results lead to B-S Law)

B-S. form

$$|d\vec{B}| \propto I |d\vec{r}'|$$

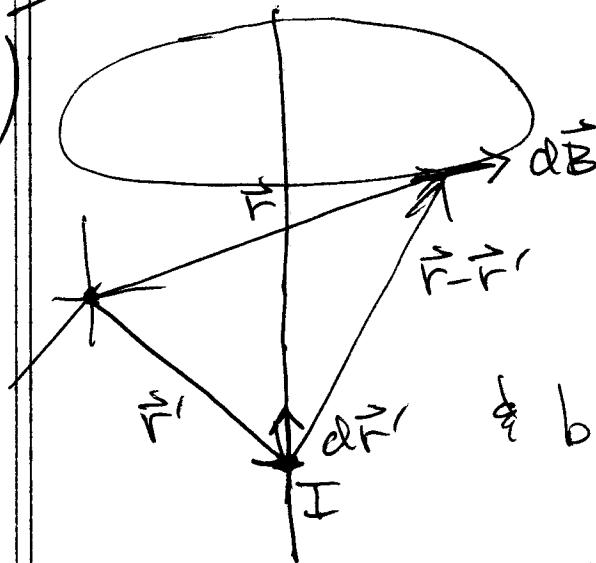
$$\propto \frac{1}{r^2}$$

I current carrying
line element $d\vec{r}'$

$$\left. \begin{aligned} d\vec{B} &\perp \text{to } d\vec{r}' \\ &\perp \text{to } (\vec{r} - \vec{r}') \end{aligned} \right\} \Rightarrow d\vec{B} \parallel d\vec{r}' \times (\vec{r} - \vec{r}')$$

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III. 1)



Law of B-S.

$$d\vec{B}(P) = \frac{\mu_0 I}{4\pi} \frac{d\vec{r} \times (\vec{r} - \vec{r}')}{|\vec{r} - \vec{r}'|^3}$$

& by superposition

$$\vec{B}(P) = \frac{\mu_0}{4\pi} \int_C I \frac{d\vec{r}' \times (\vec{r} - \vec{r}')}{|\vec{r} - \vec{r}'|^3}$$

μ_0 = permeability of free space

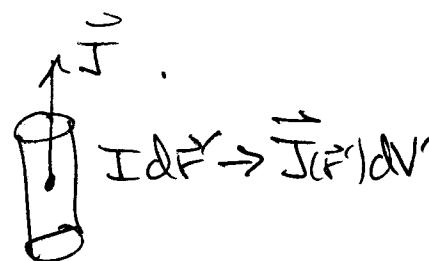
$$= 4\pi \times 10^{-7} \frac{\text{kg} \cdot \text{m}}{\text{A} \cdot \text{s}^2}$$

$$\left(= \frac{\mu_0}{4\pi} \int_C I \frac{d\vec{l} \times \hat{n}}{l^2} \right)$$

$$\frac{\text{nt}}{\text{amp}^2} = \frac{\text{Tesla}}{\text{amp}}$$

I if current flowing in matter

$$I d\vec{r}' \rightarrow \vec{J}(P') dV'$$



Surface $I d\vec{r}' \rightarrow \vec{J}(P') dS'$

B-S law

$$\vec{B}(P) = \frac{\mu_0}{4\pi} \int dV' \frac{\vec{J}(P') \times (\vec{r} - \vec{r}')}{|\vec{r} - \vec{r}'|^3}$$

$$d\vec{B}(P) = \frac{\mu_0}{4\pi} \frac{\vec{J}(P') \times (\vec{r} - \vec{r}')}{|\vec{r} - \vec{r}'|^3} dV'$$

IV. 2.) Consistency: $\vec{\nabla} \cdot \vec{B}(F) = 0$ check

$$\vec{\nabla} \cdot \vec{B}(F) = \frac{\mu_0}{4\pi} \int dV'$$

$$\vec{\nabla}_{r'} \cdot \left[\frac{\vec{j}(F') \times (\vec{F} - \vec{r}')}{|\vec{F} - \vec{r}'|^3} \right]$$

use

$$\vec{\nabla} \cdot (\vec{A} \times \vec{B}) = -\vec{A} \cdot (\vec{\nabla} \times \vec{B}) + \vec{B} \cdot (\vec{\nabla} \times \vec{A})$$

but $\vec{\nabla}_F \times \vec{j}(F) = 0$ i.e. $\frac{\partial}{\partial x_{y,z}}$ not x,y,z .

So

$$\vec{\nabla} \cdot \vec{B}(F) = - \frac{\mu_0}{4\pi} \int dV' \vec{j}(F') \cdot \vec{\nabla}_F \times \left(\frac{\vec{F} - \vec{r}'}{|\vec{F} - \vec{r}'|^3} \right)$$

$$\text{Now } \frac{\vec{F} - \vec{r}'}{|\vec{F} - \vec{r}'|^3} = -\vec{\nabla} \left(\frac{1}{|\vec{F} - \vec{r}'|} \right)$$

$$\text{i.e. } \frac{\partial}{\partial x} \frac{1}{|\vec{F} - \vec{r}'|} = \frac{\partial}{\partial x} \frac{1}{\sqrt{(x-x')^2 + (y-y')^2 + (z-z')^2}}$$

$$= -\frac{1}{2} \frac{1}{|\vec{F} - \vec{r}'|^3} \frac{\partial}{\partial x} |\vec{F} - \vec{r}'|^3$$

$$= -\frac{x - x'}{|\vec{F} - \vec{r}'|^3} \text{ etc.}$$

But

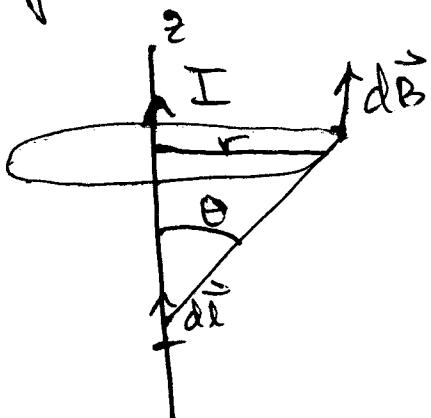
$$\vec{\nabla} \times \vec{\nabla} f = 0!$$

$$\Rightarrow \boxed{\vec{\nabla} \cdot \vec{B}(F) = 0}$$

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II. b.) Examples:

1)

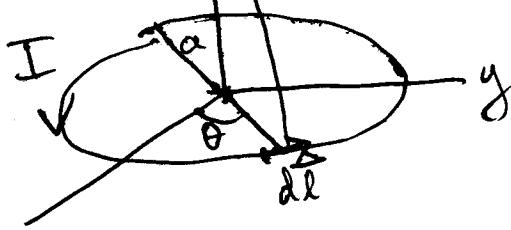


$$|\vec{B}| = \frac{\mu_0 I}{2\pi r}$$

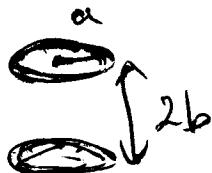
2) Circular loop

P

$$\vec{B}(z) = \frac{\mu_0 I}{2\pi} \frac{a^2}{(z^2 + a^2)^{3/2}} \hat{k}$$

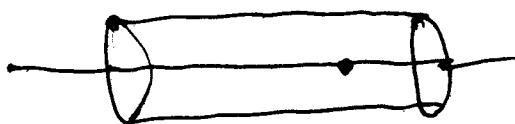


3) Helmholtz Coils



use circular loop
case

4) Solenoid : field on axis



messy: compare
circular loop
case.

- -

I.1) Ampere's (Circuital) Law

B-S law was for steady currents:

current flows in wire steadily — no charge builds up just keeps flowing $\frac{d\rho}{dt} = 0$
 $\Rightarrow \vec{\nabla} \cdot \vec{J} = 0$ from continuity eq.

Under these conditions we find simple expression for $\vec{\nabla} \times \vec{B}$:

$$\vec{\nabla}_F \times \vec{B}(F) = \frac{\mu_0}{4\pi} \int_V dV' \vec{\nabla}_{F'} \times \left[\frac{\vec{J}(F') \times (F - F')}{|F - F'|^3} \right]$$

Use

$$\vec{\nabla} \times (\vec{F} \times \vec{G}) = (\vec{\nabla} \cdot \vec{G}) \vec{F} - (\vec{F} \cdot \vec{G}) \vec{G} + (\vec{G} \cdot \vec{\nabla}) \vec{F} - (\vec{F} \cdot \vec{\nabla}) \vec{G}$$

with $\vec{F} = \vec{J}(F')$ $\Rightarrow \frac{\partial}{\partial x_i} \vec{J}(F') = 0$

$$\vec{G} = \frac{\vec{F} - \vec{F}'}{|F - F'|^3} \Rightarrow$$

$$\begin{aligned} \vec{\nabla}_F \times \vec{B}(F) &= \frac{\mu_0}{4\pi} \int_V dV' \left\{ \vec{J}(F') \left(\vec{\nabla}_F \cdot \frac{\vec{F} - \vec{F}'}{|F - F'|^3} \right) \right. \\ &\quad \left. - \vec{J}(F') \cdot \vec{\nabla}_F \left(\frac{\vec{F} - \vec{F}'}{|F - F'|^3} \right) \right\} \end{aligned}$$

$$\text{But } \mathbf{1) } \frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|^3} = -\vec{\nabla}_{\vec{r}} \left(\frac{1}{|\vec{r} - \vec{r}'|} \right) \quad \rightarrow$$

hence

$$\vec{\nabla}_{\vec{r}} \cdot \left(\frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|^3} \right) = -\vec{\nabla}_{\vec{r}}^2 \left(\frac{1}{|\vec{r} - \vec{r}'|} \right)$$

$$= -(-4\pi \delta^3(\vec{r} - \vec{r}'))$$

$$= 4\pi \delta^3(\vec{r} - \vec{r}')$$

$$\text{So the first term RHS} = \frac{\mu_0}{4\pi} \int dV' \vec{J}(\vec{r}') \cdot 4\pi \delta^3(\vec{r} - \vec{r}') \\ = \mu_0 \vec{J}(\vec{r}) .$$

Second term:

$$\text{2) } \vec{J}(\vec{r}') \cdot \vec{\nabla}_{\vec{r}} \left(\frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|^3} \right) = -\vec{J}(\vec{r}') \cdot \vec{\nabla}_{\vec{r}'} \left(\frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|^3} \right) \\ = +\vec{J}(\vec{r}') \cdot \vec{\nabla}_{\vec{r}'} \frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|^3}$$

$$\text{But } \vec{\nabla} \cdot (\varphi \vec{F}) = (\vec{\nabla} \varphi) \cdot \vec{F} + \varphi \vec{\nabla} \cdot \vec{F}$$

$$\Rightarrow \vec{\nabla}_{\vec{r}'} \cdot \left(\vec{J}(\vec{r}') \frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|^3} \right) = \frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|^3} \vec{\nabla}_{\vec{r}'} \cdot \vec{J}(\vec{r}') \xrightarrow[\text{Steady current}]{} \\ + \vec{J}(\vec{r}') \cdot \vec{\nabla}_{\vec{r}'} \left(\frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|^3} \right)$$

Similarly for y, z .

→
- II 2) So

$$\begin{aligned} & \int_V \vec{J}(F') \cdot \vec{\nabla}_{F'} \left(\frac{x' - x}{|F' - F|^3} \right) dV' \\ &= \int_V dV' \vec{\nabla}_{F'} \cdot \left(\vec{J}(F') \frac{x' - x}{|F' - F|^3} \right) \\ &= \oint_S \frac{x' - x}{|F' - F|^3} \vec{J}(F') \cdot d\vec{S}' \equiv 0. \end{aligned}$$

Let S lie outside volume V so $\vec{J} = 0$ on S .

Thus $\int_V \vec{J}(F') \cdot \vec{\nabla}_{F'} \frac{F' - F}{|F' - F|^3} dV' = 0.$

$$\Rightarrow \boxed{\vec{\nabla} \times \vec{B}(F) = \mu_0 \vec{J}(F)}$$

Amperé's Law
(differential form)

3) Integrate over open surface & use Stokes' Theorem

$$\int_S \vec{\nabla} \times \vec{B} \cdot d\vec{S} = \oint_C \vec{B} \cdot d\vec{l} = \mu_0 \int_S \vec{J} \cdot d\vec{S}$$

↑
open surface ↑
closed curve of S
= boundary of S

- II. 3.) But $I = \int_S \vec{J} \cdot d\vec{S}$ = total current flowing thru S i.e thru C. \rightarrow

So

$$\oint_C \vec{B} \cdot d\vec{l} = \mu_0 I$$

integral form
of Ampere's law.

III. Magneto-statics : $\frac{d\phi}{dt} = 0 = \nabla \cdot \vec{J}$

$$\nabla \times \vec{B} = \mu_0 J \quad \text{Ampere's law}$$

Also $\nabla \cdot \vec{B} = 0$ Fundamental law of magnetism

Electrostatics $\nabla \cdot \vec{E} = \frac{1}{\epsilon_0} \rho$ Gauss's law

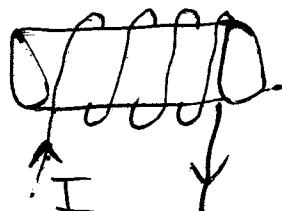
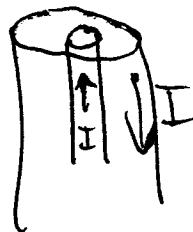
$$\nabla \times \vec{E} = 0$$

$$F = q(\vec{E} + \vec{v} \times \vec{B})$$

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Ex. Ampere's law

- 1) $\oint \mathbf{B} \cdot d\mathbf{l}$ wire
- 2) Coaxial cable
- 3) Solenoid



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i) VII.) Magnetic Vector Potential

Thm. 1
p. 57

$$\vec{\nabla} \times \vec{E} = 0 \Rightarrow \vec{E} = -\vec{\nabla} V.$$

scalar potential. V

Thm. 2
p. 57

$$\vec{\nabla} \cdot \vec{B} = 0 \Rightarrow \vec{B} = \vec{\nabla} \times \vec{A}$$

vector potential \vec{A} .

$$1) \vec{\nabla} \cdot \vec{B} = \vec{\nabla} \cdot (\vec{\nabla} \times \vec{A}) = 0 \quad \checkmark$$

$$2) \vec{\nabla} \times \vec{B} = \mu_0 \vec{J} = \vec{J} \times (\vec{\nabla} \times \vec{A})$$

$$\text{but } \vec{\nabla} \times (\vec{\nabla} \times \vec{A}) = \vec{\nabla}(\vec{\nabla} \cdot \vec{A}) - \vec{\nabla}^2 \vec{A}$$

\vec{A}

Notice we can add $\vec{\nabla} \lambda (\neq)$ to

$$\vec{A}' = \vec{A} + \vec{\nabla} \lambda \quad \text{gauge transformation}$$

$$\begin{aligned} \vec{B}' &= \vec{\nabla} \times \vec{A}' = \vec{\nabla} \times \vec{A} + \underbrace{\vec{\nabla} \times \vec{\nabla} \lambda}_{=0} \\ &= \vec{B} \quad \checkmark \end{aligned}$$

We can choose λ for our convenience — \rightarrow We can use λ to force $\vec{\nabla} \cdot \vec{A}' = 0$ even if $\vec{\nabla} \cdot \vec{A} \neq 0$
 $= f(F)$

$$\begin{aligned} \text{So } \vec{\nabla} \cdot \vec{A}' &= \vec{\nabla} \cdot \vec{A} + \vec{\nabla} \cdot \vec{\nabla} \lambda \\ &= f(F) + \vec{\nabla}^2 \lambda \end{aligned}$$

- (2 -

- VII.) $\Rightarrow \nabla^2 A(\vec{r}) = -f(\vec{r})$ Poisson's eq.

If $f \rightarrow 0$ as $|\vec{r}| \rightarrow \infty$ $\Rightarrow A(\vec{r}) = \frac{1}{4\pi} \int dV' \frac{f(\vec{r}')}{|\vec{r}-\vec{r}'|}$

$$= \frac{1}{4\pi} \int dV' \frac{\vec{\nabla}_{\vec{r}'} \cdot \vec{A}(\vec{r}')}{|\vec{r}-\vec{r}'|}$$

(if $\vec{\nabla} \cdot \vec{A}$ does not drop off we other mean to find $A(\vec{r})$ always possible).

Then we can always choose $A(\vec{r})$

so that $\vec{\nabla} \cdot \vec{A} = 0$ & $\vec{\nabla} \times \vec{B} = \vec{\nabla} \times \vec{A}$

This is called choosing a gauge; the gauge is called the Coulomb gauge $\vec{\nabla} \cdot \vec{A} = 0$.

But $\vec{\nabla} \cdot \vec{A} = 0 \Rightarrow$

$$\vec{\nabla} \times (\vec{\nabla} \times \vec{A}) = \vec{\nabla} (\vec{\nabla} \cdot \vec{A}) = \vec{\nabla}^2 \vec{A}$$

Please

$$\boxed{\nabla^2 \vec{A}(\vec{r}) = -\mu_0 \vec{J}(\vec{r})}$$

again 3 Poisson's equations x, y, z components

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VII. 1) Assuming $\vec{J} \rightarrow 0$ as $(\vec{r}_1 \rightarrow \infty)$

$$\Rightarrow \boxed{A(\vec{r}) = \frac{\mu_0}{4\pi} \int dV' \frac{\vec{J}(\vec{r}')}{|\vec{r} - \vec{r}'|}}$$

First

Alternate derivation: B-S-law

$$B(\vec{r}) = \frac{\mu_0}{4\pi} \int dV' \frac{\vec{J}(\vec{r}') \times (\vec{r} - \vec{r}')}{|\vec{r} - \vec{r}'|^3}$$

As usual $\frac{\vec{r} - \vec{r}'}{|\vec{r} - \vec{r}'|^3} = -\vec{\nabla}_{\vec{r}'} \frac{1}{|\vec{r} - \vec{r}'|}$

$$\vec{\nabla} \times (\varphi \vec{F}) = \varphi \vec{\nabla} \times \vec{F} - \vec{F} \times \vec{\nabla} \varphi$$

$$\Rightarrow \vec{\nabla}_{\vec{r}} \times \left[\frac{1}{|\vec{r} - \vec{r}'|} \vec{J}(\vec{r}') \right] = -\vec{J}(\vec{r}') \times \vec{\nabla}_{\vec{r}} \frac{1}{|\vec{r} - \vec{r}'|}$$

So

$$B(\vec{r}) = \frac{\mu_0}{4\pi} \int dV' \vec{\nabla}_{\vec{r}'} \times \left[\frac{\vec{J}(\vec{r}')}{|\vec{r} - \vec{r}'|} \right]$$

$$= \vec{\nabla}_{\vec{r}} \times \left[\frac{\mu_0}{4\pi} \int dV' \frac{\vec{J}(\vec{r}')}{|\vec{r} - \vec{r}'|} \right]$$

$$= \vec{A}(\vec{r}) \quad \checkmark$$

definition $\Rightarrow \vec{\nabla} \cdot \vec{A} = 0$ curl-gauge-

VII. 2) For line currents

$$\vec{A}(F) = \frac{\mu_0 I}{4\pi} \int_C \frac{d\vec{r}'}{|F - \vec{r}'|}$$

Surface Currents

$$\vec{A}(F) = \frac{\mu_0}{4\pi} \int_S \frac{\vec{K}(F') dS'}{|F - \vec{r}'|}$$

3) Mathematical Aside: If $\vec{D} \cdot \vec{B} = 0$ then

$$\vec{B} = \vec{\nabla} \times \vec{A} \text{ for some } \vec{A}.$$

Proof by Construction of \vec{A}

$$\vec{\nabla} \times \vec{A} = \vec{B} \quad \left\{ \begin{array}{l} \partial_y A_z - \partial_z A_y = B_x \\ \partial_z A_x - \partial_x A_z = B_y \\ \partial_x A_y - \partial_y A_x = B_z \end{array} \right.$$

Given \vec{B}

\vec{A} is not unique — gauge transformations

$$\vec{A}' = \vec{A} + \vec{\nabla} \lambda \Rightarrow \vec{B}' = \vec{B}$$

So choose λ so that $A_x = 0 \Rightarrow A'_x = \partial_x \lambda$

$$\Rightarrow \lambda = \int_0^x dx' A'_x(x',y,z) + \lambda(y,z)$$

Then

$$\partial_x A_y = B_z \Rightarrow A_y = \int_0^x dx' B_z(x', y, z) + C_y(y, z)$$

$$-\partial_x A_z = B_y \Rightarrow -A_z = \int_0^x dx' B_y(x', y, z) - C_z(y, z)$$

$$\text{Now } \partial_y A_z - \partial_z A_y = B_x$$

$$= - \int_0^x dx' \partial_y B_y(x', y, z) + \partial_y C_z(y, z)$$

$$- \int_0^x dx' \partial_z B_z(x', y, z) - \partial_z C_y(y, z) = B_x$$

$$\text{But } \vec{\nabla} \cdot \vec{B} = 0 = \partial_x B_x + \partial_y B_y + \partial_z B_z$$

\Rightarrow

$$B_x = \int_0^x dx' (\partial_x B_x(x', y, z) + \partial_y B_y(x', y, z))$$

$$- \int_0^x dx' \partial_y B_y(x', y, z) + \partial_y C_z - \partial_z C_y$$

$$B_x(x, y, z) = B_x(0, y, z) - B_x(0, y, z) + \partial_y C_z - \partial_z C_y$$

$$\Rightarrow \boxed{\partial_y C_z(y, z) - \partial_z C_y(y, z) = +B_x(0, y, z)}$$

Again use λ -gauge invariance

$$\tilde{A}'' = \vec{A} + \vec{\nabla} \lambda \quad \left\{ \begin{array}{l} A''_x = A_x + \partial_x \lambda \\ A''_y = A_y + \partial_y \lambda \\ A''_z = A_z + \partial_z \lambda \end{array} \right. \quad \lambda = \lambda(y, z)$$

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to choose $C_y = 0$. That is the equation

$$\partial_y C_z - \partial_z C_y = B_x$$

remains unchanged if $C'_z = C_z + \partial_z \lambda$
 $C'_y = C_y + \partial_y \lambda$

$\lambda = \lambda(y, z)$; choose $\lambda \ni C_y = 0$
i.e.

$$\partial_y \lambda = -C_y \Rightarrow \lambda(y, z) = - \int_0^y \partial_y' C_y(y', z) + l(z)$$

So

$$\partial_y C_z|_{y,z} = B_x(0, y, z)$$

and

$$C_z(y, z) = \int_0^y \partial_y' B_x(0, y', z) + C(z)$$

Hence

$$A_x = 0$$

$$A_y = \int_0^x dx' B_z(x', y, z)$$

$$A_z = + \int_0^y dy' B_x(0, y', z)$$

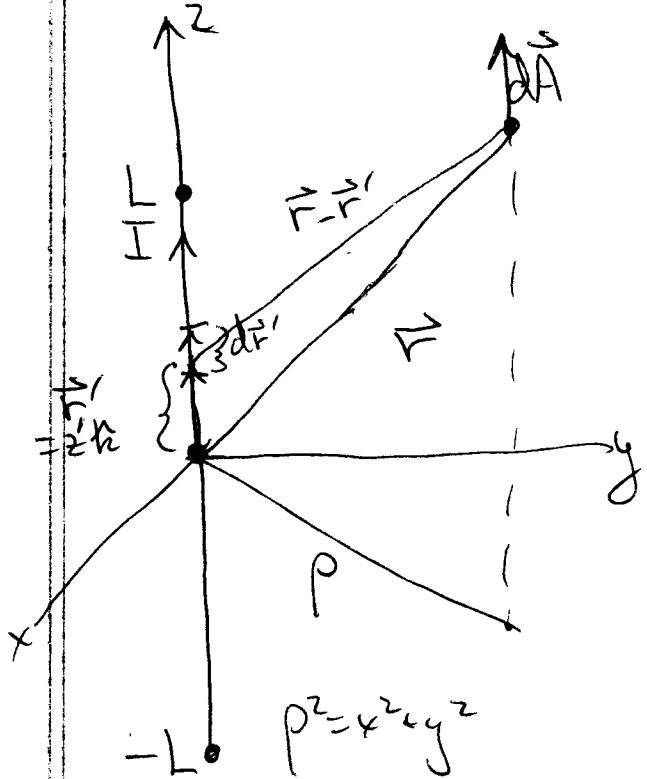
$$- \int_0^x dx' B_y(x', y, z) + C(z)$$

Use final gauge invariance $l(z)$ to set $C=0$.

So \exists an \vec{A} for every \vec{B} with $\vec{\nabla} \cdot \vec{B} = 0$
 $\Rightarrow \vec{B} = \vec{\nabla} \times \vec{A}$.

We finally can add to \vec{A} any other \vec{D} to recover general formula $\vec{B} = \vec{\nabla} \times \vec{A}$ for unstrained \vec{A} i.e. could chose Coulomb gauge for instance $\vec{\nabla} \cdot \vec{A} = 0$.

VII, 4) Example: Calculate \vec{A} due to a finite length, steady current carrying wire



$$\begin{aligned}\vec{A}(r) &= \frac{\mu_0 I}{4\pi} \int_{-L}^L \frac{dz' \hat{z}}{|\vec{r} - \vec{r}'|} \\ &= \frac{\mu_0 I k}{4\pi} \int_{-L}^{+L} \frac{dz'}{\sqrt{x^2 + y^2 + (z - z')^2}} \\ &= \frac{\mu_0 I k}{4\pi} \int_{u=-L-z}^{u=L-z} \frac{du}{\sqrt{x^2 + y^2 + u^2}} \\ &\quad (u = z' - z ; du = dz')\end{aligned}$$

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Now

$$\int \frac{du}{\sqrt{p^2+u^2}} = \ln [u + \sqrt{p^2+u^2}]$$

check

$$\begin{aligned} \frac{d}{du} \left(\ln [u + \sqrt{p^2+u^2}] \right) &= \frac{1}{u + \sqrt{p^2+u^2}} \left(1 + \frac{1}{2} \frac{2u}{\sqrt{p^2+u^2}} \right) \\ &= \frac{1}{u + \sqrt{p^2+u^2}} \left(\frac{\sqrt{p^2+u^2} + u}{\sqrt{p^2+u^2}} \right) \\ &= \frac{1}{\sqrt{p^2+u^2}} \quad \checkmark. \end{aligned}$$

So

$$\vec{A}_{(F)} = \frac{\mu_0 I k}{4\pi} \ln \left[u + \sqrt{p^2+u^2} \right] \Big|_{u=-L-z}^{u=L-z}$$

$$= \frac{\mu_0 I k}{4\pi} \ln \left[\frac{L-z + \sqrt{x^2+y^2+(L-z)^2}}{-L-z + \sqrt{x^2+y^2+(L+z)^2}} \right]$$

$$= \frac{\mu_0 I k}{4\pi} \ln \left[\frac{(L-z) \left[1 + \sqrt{1 + \frac{x^2+y^2}{(L-z)^2}} \right]}{(L+z) \left[-1 + \sqrt{1 + \frac{x^2+y^2}{(L+z)^2}} \right]} \right]$$

Note for $L \gg x, y, z$

$$\vec{A}_{(F)} \approx \frac{\mu_0 I k}{4\pi} \ln \left[\frac{L \left[1 + 1 \right]}{L \left[-1 + 1 + \frac{1}{2} \frac{x^2+y^2}{(L)^2} \right]} \right]$$

$$\approx \frac{\mu_0 I k}{4\pi} \ln \frac{4L^2}{(x^2+y^2)} \approx \frac{\mu_0 I k}{2\pi} \ln \left(\frac{2L}{\rho} \right)$$

$$\text{So } \vec{A}(\vec{r}) \approx \frac{\mu_0 I \hat{h}}{2\pi} \ln\left(\frac{2L}{\rho}\right) \rightarrow \infty \text{ as } L \rightarrow \infty$$

But still \vec{B} is finite as $L \rightarrow \infty$. We can find \vec{B} for finite L , then take the limit

$$\vec{B}(\vec{r}) = \vec{\nabla} \times \vec{A}(\vec{r}) ; \text{ in cylindrical coordinates}$$

This is

$$\begin{aligned} \vec{B}(\vec{r}) &= \left[\frac{1}{\rho} \frac{\partial A_z}{\partial \varphi} - \frac{\partial A_\varphi}{\partial z} \right] \hat{\rho} + \left[\frac{\partial A_\varphi}{\partial z} - \frac{\partial A_z}{\partial \rho} \right] \hat{\varphi} \\ &\quad + \frac{1}{\rho} \left[\frac{z}{\partial \rho} (\rho A_\varphi) - \frac{\partial A_\varphi}{\partial \rho} \right] \hat{z} \end{aligned}$$

But $A_\rho = A_\varphi = 0$ and

$$A_z = \frac{\mu_0 I}{4\pi} \ln \left[\frac{(L-z) \left[1 + \sqrt{1 + \frac{\rho^2}{(L-z)^2}} \right]}{(L+z) \left[-1 + \sqrt{1 + \frac{\rho^2}{(L+z)^2}} \right]} \right]$$

$$\text{Since } \frac{\partial A_z}{\partial \varphi} = 0 \Rightarrow \boxed{\vec{B}(\vec{r}) = -\frac{\partial A_z}{\partial \rho} \hat{\varphi}}$$

For $L \gg \rho, z$

$$\begin{aligned} A_z &\approx \frac{\mu_0 I}{2\pi} \ln\left(\frac{2L}{\rho}\right) \Rightarrow \vec{B}(\vec{r}) \approx -\frac{\mu_0 I \hat{h}}{2\pi} \frac{\rho}{2L} \left(-\frac{2L}{\rho^2}\right) \\ &\approx \frac{\mu_0 I}{2\pi \rho} \hat{\varphi} \end{aligned}$$

So $\vec{B}(\vec{r}) \approx \frac{\mu_0 I}{2\pi r} \hat{\phi}$ and as $L \rightarrow \infty$
is finite and

becomes

$$\vec{B}(\vec{r}) = \frac{\mu_0 I}{2\pi \sqrt{x^2 + y^2}} \hat{\phi} \text{ as we}$$

obtained directly earlier.

VII.5) Finally, notice that $\vec{\nabla} \cdot \vec{B} = 0$; $\vec{\nabla} \times \vec{B} = \mu_0 \vec{J}$

$$\Rightarrow \vec{\nabla} \times \vec{\nabla} \times \vec{B} = \mu_0 \vec{\nabla} \times \vec{J}$$

$$= \vec{\nabla} (\vec{\nabla} \cdot \vec{B}) - \vec{\nabla}^2 \vec{B} = -\vec{\nabla}^2 \vec{B} = \mu_0 \vec{\nabla} \times \vec{J}$$

So $\vec{B}(\vec{r}) = \frac{\mu_0}{4\pi} \int dV' \frac{\vec{\nabla}_{r'} \cdot \vec{J}(\vec{r}')}{|\vec{r} - \vec{r}'|}$.

Again $\vec{\nabla} \times (\varphi \vec{F}) = \varphi \vec{\nabla} \times \vec{F} - \vec{F} \times \vec{\nabla} \varphi$

$$\Rightarrow \vec{B}(\vec{r}) = \frac{\mu_0}{4\pi} \int dV' \vec{\nabla}_{r'} \times \left(\frac{\vec{J}(\vec{r}')}{|\vec{r} - \vec{r}'|} \right)$$

+ $\frac{\mu_0}{4\pi} \int dV' \vec{J}(\vec{r}') \times \vec{\nabla}_{r'} \frac{1}{|\vec{r} - \vec{r}'|}$ surface term

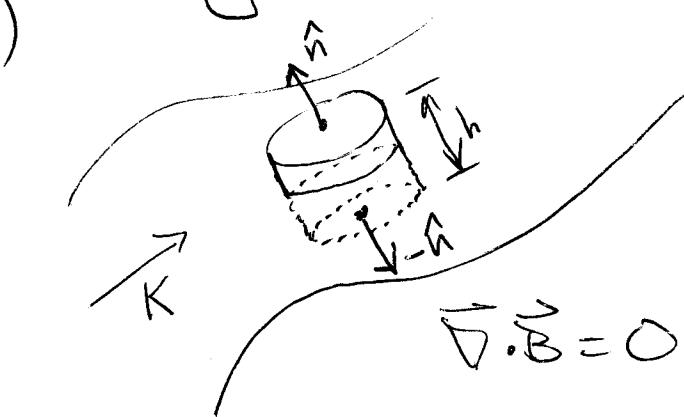
$$= + \frac{\mu_0}{4\pi} \int dV' \frac{\vec{J}(\vec{r}') \times (\vec{r} - \vec{r}')}{|r - r'|^3}$$

The
Biot-Savart law

Likewise $\vec{\nabla} \cdot \vec{A} = 0$ Coulomb gauge and $\vec{\nabla} \times \vec{A} = \vec{B}$

$$\Rightarrow \vec{A}(\vec{r}) = \frac{1}{4\pi} \int dV' \frac{\vec{B}(\vec{r}') \times (\vec{r} - \vec{r}')}{| \vec{r} - \vec{r}' |^3}$$

VIII. Boundary Conditions:



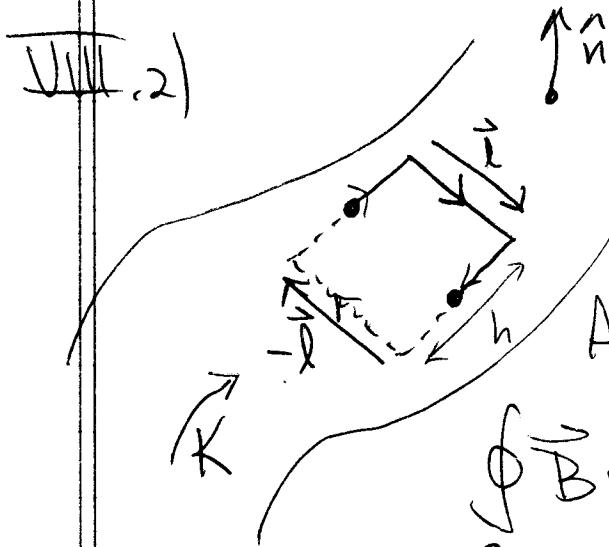
$$\vec{\nabla} \cdot \vec{B} = 0 \Rightarrow \oint_S \vec{B} \cdot d\vec{s} = 0$$

$$= (\vec{B} \cdot \vec{n})_{\text{above}} - (\vec{B} \cdot \vec{n})_{\text{below}}) \Delta a.$$

$$+ \int_{\text{cylinder height}} \vec{B} \cdot d\vec{s} \sim O(h) \rightarrow 0$$

$$\Rightarrow \boxed{B_{\perp \text{above}} = B_{\perp \text{below}}}$$

The normal component of \vec{B} across any surface is continuous.



Consider amperian loop

Amper's law

$$\oint_C \vec{B} \cdot d\vec{l} = \mu_0 I_{enc.}$$

$$I_{enc} = \vec{K} \cdot (\hat{n} \times \vec{l})$$

$$\oint_C \vec{B} \cdot d\vec{l} = (\vec{B}_{\text{above}} - \vec{B}_{\text{below}}) \cdot \vec{l}$$

$$+ \underbrace{\int_{\text{Sides}} \vec{B} \cdot d\vec{l}}$$

$$\approx 0(h) \rightarrow 0.$$

Thus

$$(\vec{B}_{\text{above}} - \vec{B}_{\text{below}}) \cdot \vec{l} = \mu_0 \vec{K} \cdot (\hat{n} \times \vec{l})$$

$$\text{using } \vec{K} \cdot (\hat{n} \times \vec{l}) = \vec{l} \cdot (\vec{K} \times \hat{n})$$

\Rightarrow

$$(\vec{B}_{\text{above}} - \vec{B}_{\text{below}}) \cdot \vec{l} = \vec{l} \cdot (\mu_0 \vec{K} \times \hat{n})$$

The tangential component of \vec{B} is discontinuous across a surface with current density.

Since $\vec{B} \cdot \hat{n}$ above = $\vec{B} \cdot \hat{n}$ below we can sum up all conditions as $\vec{B}_{\text{above}} - \vec{B}_{\text{below}} = \mu_0 (\vec{k} \times \hat{n})$ -23-

That is since \vec{l} is any vector in boundary surface

$$(\vec{B}_{\text{above}} - \vec{B}_{\text{below}})_{\text{tangential}} = \mu_0 \vec{k} \times \hat{n}$$

* Component vector

Or taking the cross-product with \hat{n}

$$\hat{n} \times (\vec{B}_{\text{above}} - \vec{B}_{\text{below}}) = \mu_0 \vec{k}$$

VIII. 3.) Vector potential \vec{A} is continuous across the boundary

$$1) \vec{\nabla} \cdot \vec{A} = 0 \Rightarrow (\vec{A}_{\text{above}} - \vec{A}_{\text{below}}) \cdot \hat{n} = 0$$

$$2) \vec{\nabla} \times \vec{A} = \vec{B}$$

$$\Rightarrow \oint \vec{A} \cdot d\vec{l} = \iint_S \vec{B} \cdot d\vec{S} = \Phi = \text{magnetic flux}$$

but for a superthin loop of vanishing thickness the flux is zero through it

Since area $\rightarrow 0$

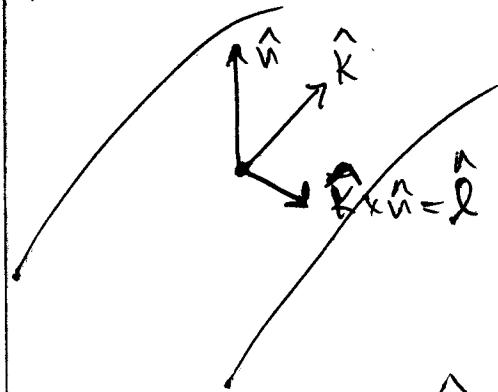
$$\Rightarrow (\vec{A}_{\text{above}} - \vec{A}_{\text{below}})_{\text{tangential}} = 0$$

$$\Rightarrow \boxed{\vec{A}_{\text{above}} = \vec{A}_{\text{below}}} \quad \begin{matrix} \text{like } V \\ \text{in electrostatics} \end{matrix}$$

III. b) Now since $\vec{B} = \vec{\nabla} \times \vec{A}$ we have

$$\vec{B}_{\text{above}} - \vec{B}_{\text{below}} = \vec{\nabla} \times \vec{A}_{\text{above}} - \vec{\nabla} \times \vec{A}_{\text{below}} \\ = \mu_0 (\vec{K} \times \hat{n})$$

But



$$\text{but } \Delta \vec{r} = \Delta r \hat{k} + \Delta_{kn} \hat{K} \times \hat{n}$$

\vec{A} is continuous so moving along surface

$$\vec{A}(\vec{r} + \Delta \vec{r}) = \vec{A}_{\text{above}}(\vec{r}) + \vec{B} \cdot \vec{\nabla} \vec{A}_{\text{above}} \Big|_{\text{surface}} \\ = \vec{A}_{\text{below}}(\vec{r} + \Delta \vec{r}) \\ = \vec{A}_{\text{below}}(\vec{r}) + \vec{B} \cdot \vec{\nabla} \vec{A}_{\text{below}} \Big|_{\text{surface}}$$

$$\frac{\partial \vec{A}}{\partial k}, \frac{\partial \vec{A}}{\partial (K \times n)} = \frac{\partial \vec{A}}{\partial l} \text{ is}$$

continuous

So only $\frac{\partial \vec{A}}{\partial n}$ can be discontinuous. But

$$\vec{\nabla} \times \vec{A} = \begin{vmatrix} \hat{x} & \hat{y} & \hat{n} \\ \frac{\partial}{\partial x} & \frac{\partial}{\partial y} & \frac{\partial}{\partial n} \\ A_x & A_y & A_n \end{vmatrix} = \hat{x} \left(\frac{\partial A_n}{\partial k} - \frac{\partial A_k}{\partial n} \right) \\ - \hat{y} \left(\frac{\partial A_n}{\partial l} - \frac{\partial A_l}{\partial n} \right) + \hat{n} \left(\frac{\partial A_l}{\partial x} - \frac{\partial A_x}{\partial k} \right)$$

$$\vec{\nabla} \times \vec{A}_{\text{above}} - \vec{\nabla} \times \vec{A}_{\text{below}}$$

$$= \hat{x} \left(-\frac{\partial A_k}{\partial n} \right)_{\substack{\text{above} \\ \text{- below}}} + \hat{y} \left(\frac{\partial A_l}{\partial n} \right)_{\substack{\text{above} \\ \text{- below}}} = \mu_0 K \hat{l} \Rightarrow$$

$$\frac{\partial A_l}{\partial n} \Big|_{\substack{\text{above} \\ \text{below}}} = 0 \\ \frac{\partial A_k}{\partial n} \Big|_{\substack{\text{above} \\ \text{- below}}} = -\mu_0 K$$

(VIII.) 3) So

$$\left. \frac{\partial \vec{A}}{\partial n} \right|_{\text{above}} = -\mu_0 K + \left. \frac{\partial \vec{A}}{\partial n} \right|_{\text{below}}$$

So

$$\left. \frac{\partial \vec{A}}{\partial n} \right|_{\text{above}} - \left. \frac{\partial \vec{A}}{\partial n} \right|_{\text{below}} = -\mu_0 \vec{K}$$

Note: we used Coulomb gauge

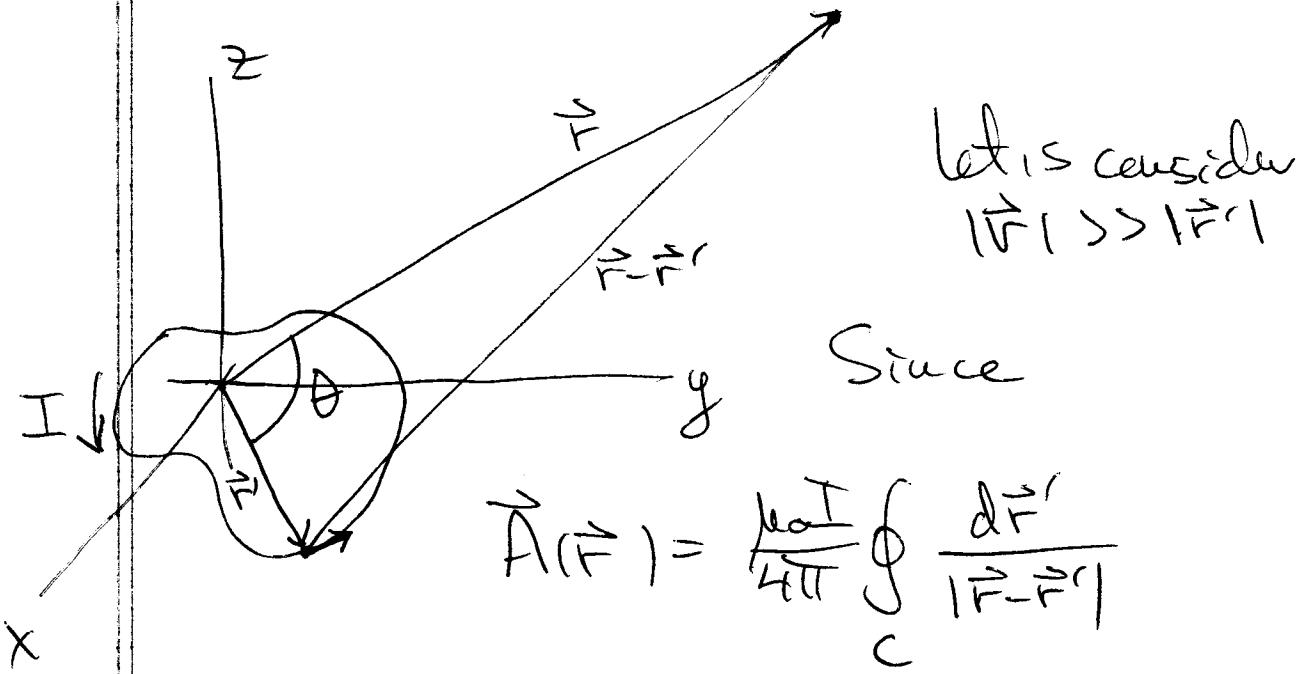
$$0 = \vec{\nabla} \cdot \vec{A} = \left(\frac{\partial A_e}{\partial e} + \frac{\partial A_K}{\partial K} + \left. \frac{\partial A_n}{\partial n} \right|_{\text{above}} \right) \\ = \left(\frac{\partial A_e}{\partial e} + \frac{\partial A_K}{\partial K} + \left. \frac{\partial A_n}{\partial n} \right|_{\text{below}} \right)$$

but $\frac{\partial \vec{A}}{\partial e}$, $\frac{\partial \vec{A}}{\partial K}$ are continuous \Rightarrow

$$\left. \frac{\partial A_n}{\partial n} \right|_{\text{above}} = \left. \frac{\partial A_n}{\partial n} \right|_{\text{below}}$$

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IX.) Multipole Expansion For The Vector Potential



We can consider expanding $\frac{1}{|\vec{r} - \vec{r}'|}$
in powers of $\frac{|r'|}{|r|}$.

Now

$$\begin{aligned}
 \frac{1}{|\vec{r} - \vec{r}'|} &= \frac{1}{\sqrt{\vec{r} \cdot \vec{r} + \vec{r}' \cdot \vec{r}' - 2\vec{r} \cdot \vec{r}'}} \\
 &= \frac{1}{\sqrt{r^2 + r'^2 - 2rr' \cos\theta}} \\
 &= \frac{1}{r} \frac{1}{\sqrt{1 + \frac{r'^2}{r^2} - 2\frac{r'}{r} \cos\theta}}
 \end{aligned}$$

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But the square root we are familiar with from the multiple expansion in electrostatics

$$\frac{1}{|\vec{r} - \vec{r}'|} = \frac{1}{r} \sum_{k=0}^{\infty} \left(\frac{r'}{r}\right)^k P_k(\cos\theta)$$

$P_n(\cos\theta)$ = Legendre Polynomials.

Proof: let $\xi = \cos\theta$ and $t = \frac{r'}{r} < 1$

So

$$\begin{aligned} \frac{1}{|\vec{r} - \vec{r}'|} &= \frac{1}{r} \frac{1}{\sqrt{1 - 2\frac{r'}{r}\cos\theta + \left(\frac{r'}{r}\right)^2}} \\ &= \frac{1}{r} \frac{1}{\sqrt{1 - 2t\xi + t^2}} = \frac{1}{r} \frac{1}{\sqrt{1-u}} \end{aligned}$$

with $u = (2t\xi - t^2)$
here

$$\frac{1}{\sqrt{1 - 2t\xi + t^2}} = Z(t) = \sum_{l=0}^{\infty} t^l P_l(\xi)$$

is the generating function for Legendre polynomials

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$$P_R(\xi) = \left. \frac{d^k Z(t)}{dt^k} \right|_{t=0}$$

Check explicitly by Taylor expanding about $t=0$

$$(1-2t\bar{\beta}+t^2)^{-1/2} = \left. \left[1 - \frac{1}{2}(1-2t\bar{\beta}+t^2)^{-3/2} (-2\bar{\beta}+2t) \right] (t) \right|_{t=0}$$

$$+ \left[-\frac{1}{2} \left(-\frac{3}{2} \right) (1-2t\bar{\beta}+t^2)^{-5/2} (-2\bar{\beta}+2t)^2 \right. \\ \left. - \frac{1}{2} (1-2t\bar{\beta}+t^2)^{-3/2} 2 \right] \left. \frac{t^2}{2} \right|_{t=0}$$

$$+ \left[-\frac{1}{2} \left(-\frac{3}{2} \right) \left(1-2t\bar{\beta}+t^2 \right)^{-7/2} (-2\bar{\beta}+2t)^3 \right.$$

$$- \frac{1}{2} \left(-\frac{3}{2} \right) \left(1-2t\bar{\beta}+t^2 \right)^{-5/2} 2(-2\bar{\beta}+2t)(2)$$

$$- \frac{1}{2} \left(1-2t\bar{\beta}+t^2 \right)^{-5/2} \left(-\frac{3}{2} \right) 2(-2\bar{\beta}+2t) \right] \left. \frac{t^3}{6} \right|_{t=0}$$

...
 $t=0$

$$= \left(-\frac{1}{2}(-2\bar{\beta}) + \left[-\frac{1}{2} \left(-\frac{3}{2} \right) (-2\bar{\beta})^2 - 1 \right] \frac{t^2}{2} \right.$$

$$+ \left[-\frac{1}{2} \left(-\frac{3}{2} \right) \left(-\frac{5}{2} \right) (-2\bar{\beta})^3 - \frac{1}{2} \left(-\frac{3}{2} \right) 2^2 (-2\bar{\beta}) \right]$$

$$- \frac{1}{2} \left(-\frac{3}{2} \right) 2(-2\bar{\beta}) \left. \frac{t^3}{6} \right|_{t=0} + \dots$$

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$$Z(t) = 1 + 3t + [3\zeta^2 - 1] \frac{t^2}{2!} + [15\zeta^3 - 9\zeta] \frac{t^3}{3!} + \dots$$

Some see that

$$P_0 = 1 \quad P_2 = 3\zeta^2 - 1$$

$$P_1 = 3 \quad P_3 = 15\zeta^3 - 9\zeta \quad \dots$$

So

$$\frac{1}{(r-r')} = \frac{1}{r} Z\left(\frac{r'}{r}\right)$$

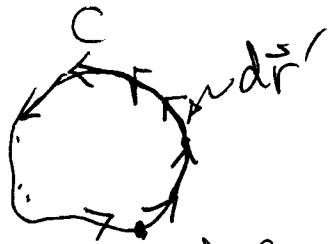
$$= \frac{1}{r} \left\{ 1 + 3 \frac{r'}{r} + [3\zeta^2 - 1] \frac{(r')^2}{2!} + \dots \right\}$$

So

$$\vec{A}(r) = \frac{\mu_0 I}{4\pi r} \left[\sum_{l=0}^{\infty} \int_C d\vec{r}' \left(\frac{r'}{r}\right)^l P_l(\cos\theta) \right]$$

$$= \frac{\mu_0 I}{4\pi r} \left[\begin{array}{l} \xrightarrow{\text{monopole}} \frac{1}{r} \int_C d\vec{r}' + \frac{1}{r^2} \int_C d\vec{r}' r' \cos\theta \\ \xrightarrow{\text{dipole}} \\ \xrightarrow{\text{quadrupole}} + \frac{1}{r^3} \int_C d\vec{r}' r'^2 \left[\frac{3}{2} \cos^2\theta - \frac{1}{2} \right] + \dots \end{array} \right]$$

Now



$$\oint_C \vec{dr}' \cdot \vec{B} = 0$$

The monopole term is zero.
This is a reflection of no magnetic charges.

V

A dipole (\vec{r})

$$\begin{aligned} \text{Now } \frac{1}{|\vec{r}-\vec{r}'|} &= \frac{1}{r} \left[\left(1 + \frac{r'^2}{r^2} - \frac{2}{r^2} \vec{r} \cdot \vec{r}' \right) \right]^{-1/2} \\ &= \frac{1}{r} \left[1 - \frac{1}{2} \frac{1}{r^2} (r'^2 - 2\vec{r} \cdot \vec{r}') + \dots \right] \\ &= \left[\frac{1}{r} + \frac{\vec{r}_0 \vec{r}'}{r^3} + O\left(\frac{r'^2}{r^3}\right) \right] \end{aligned}$$

$$A_{\text{dipole}}(\vec{r}) = \frac{\mu_0 I}{4\pi} \oint_C d\vec{r}' \frac{1}{r^2} r' \cos\theta$$

$$= \frac{\mu_0 I}{4\pi} \oint_C d\vec{r}' \frac{\vec{r}'_0 \vec{r}}{r^3}$$

$\rightarrow (-)$

So recall

$$(\vec{r}' \times d\vec{r}') \times \vec{r} = -\vec{r}' (\vec{r} \cdot d\vec{r}') + d\vec{r}' (\vec{r} \cdot \vec{r}')$$

Also

$$d[\vec{r}' (\vec{r} \cdot \vec{r}')] = \vec{r}' (\vec{r} \cdot d\vec{r}') + d\vec{r}' (\vec{r} \cdot \vec{r}')$$

So add and $\div 2$

$$d\vec{r}' (\vec{r} \cdot \vec{r}') = \frac{1}{2} (\vec{r}' \times d\vec{r}') \times \vec{r}$$

$$+ \frac{1}{2} d[\vec{r}' (\vec{r} \cdot \vec{r}')]$$

Now

$$\oint_C d[\vec{r}' (\vec{r} \cdot \vec{r}')] = 0$$

since it is the ^{total} change of a vector around a closed loop is zero — it comes back to itself.

S_0

$$\vec{A}_{\text{dipole}}(\vec{r}) = \frac{\mu_0 I}{4\pi} \frac{1}{2r^3} \oint_C (\vec{r}' \times d\vec{r}') \times \vec{r}$$

$$= \frac{\mu_0}{4\pi} \left[\frac{I}{2} \oint_C \vec{r}' \times d\vec{r}' \right] \times \frac{\vec{r}}{|\vec{r}|^3}$$

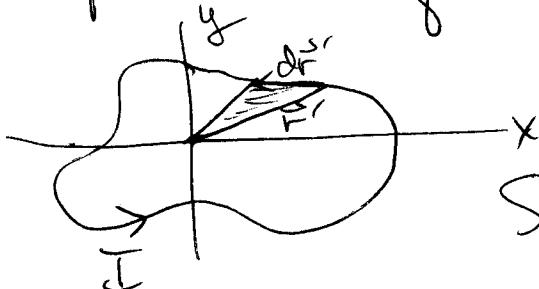
$\equiv \vec{m}$ the magnetic dipole moment

S_0

$$\vec{A}_{\text{dipole}}(\vec{r}) = \frac{\mu_0}{4\pi} \frac{\vec{m} \times \vec{r}}{r^3}$$

Valid far from coil (or let $C \rightarrow$ point, $I \rightarrow \infty$, so that $\vec{m} = \text{const.}$ and this is exact for \vec{A})

For special case of a plane loop



$$\frac{1}{2} \vec{r}' \times d\vec{r}' = \vec{da} \frac{k}{r}$$

$$S_0 \oint_C \frac{1}{2} \vec{r}' \times d\vec{r}' = \vec{a} \frac{k}{r} = \vec{a}$$

\vec{a} area of plane loop

and $\vec{m} = I \vec{a}$ independent of origin) -33-

The magnetic field for a dipole is

$$\vec{B}(F) = \frac{\mu_0}{4\pi} \nabla \times \vec{A}(F)$$

$$= \frac{\mu_0}{4\pi} \nabla \times \left[\frac{\vec{m} \times \vec{r}}{r^3} \right]$$

$$\text{Using } \nabla \times (\vec{F} \times \vec{G}) = (\vec{G} \cdot \nabla) \vec{F} - (\vec{F} \cdot \nabla) \vec{G}$$

$$+ \vec{F}(\vec{G} \cdot \nabla) - \vec{G}(\vec{F} \cdot \nabla)$$

$$\text{for } \vec{F} = \vec{m}$$

$$\vec{B} = \frac{\mu_0}{4\pi} \left[-(\vec{m} \cdot \nabla) \frac{\vec{r}}{r^3} + \vec{m} \nabla \cdot \frac{\vec{r}}{r^3} \right]$$

$$\text{Now } \nabla \cdot \frac{\vec{r}}{r^3} = \frac{3}{r^3} - \vec{r} \cdot \frac{3\vec{r}}{r^5} = \frac{3}{r^3} - \frac{3r^2}{r^5} = 0.$$

So

$$(\mu_0 \vec{m}) \frac{\vec{r}}{r^3} = \frac{\vec{m}}{r^3} - \frac{3(\vec{m} \cdot \vec{r}) \vec{r}}{r^5}$$

\Rightarrow

$$\boxed{\vec{B}_{\text{dipole}}(F) = \frac{\mu_0}{4\pi} \left[\frac{3(\vec{m} \cdot \vec{r}) \vec{r}}{r^5} - \frac{\vec{m}}{r^3} \right]}$$

(Recall electric dipole)

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$$\vec{E} = \frac{1}{4\pi\epsilon_0} \left[\frac{3(\vec{p} \cdot \vec{r})\vec{r}}{r^5} - \frac{\vec{p}}{r^3} \right]$$

So notice that in dipole case

$$\vec{E} = -\vec{\nabla}V ; V = \frac{1}{4\pi\epsilon_0} \frac{\vec{p} \cdot \vec{r}}{r^3}$$

So we can write

$$\vec{B}_{\text{dipole}} = -\mu_0 \vec{\nabla} V^*$$

$$V^* = \frac{\vec{m} \cdot \vec{r}}{4\pi r^3}$$

Magnetic scalar potential.

X.) Magnetic Material & Magnetic Intensity

a) $\vec{M} = N \langle \vec{m} \rangle = \frac{\text{average dipole moment}}{\text{volume}}$

\rightarrow magnetization $= \frac{1}{\Delta N} \sum_{\substack{\text{atoms} \\ \text{macro.} \\ \text{pt.}}}^1 \vec{m}_i$ all macroscopic magnetic properties can be described by \vec{M}

b) Magnetization Currents

$$\vec{J}_b = \vec{\nabla} \times \vec{M} \quad \text{Volume current density}$$

$$\vec{k}_b = \vec{M} \times \hat{n} \quad \text{Surface current density}$$

c) Magnetic potential & field produced by magnetized material

$$\Delta \vec{m} = \vec{M} \Delta N$$

c) and

$$\begin{aligned} d\vec{A}(\vec{r}) &= \frac{\mu_0}{4\pi} \frac{\vec{\Delta m}(\vec{r}') \times (\vec{r}-\vec{r}')}{|r-r'|^3} \\ &= \frac{\mu_0}{4\pi} \frac{\vec{M}(\vec{r}') \times (\vec{r}-\vec{r}')}{|r-r'|^3} d\sigma' \end{aligned}$$

So

$$\vec{A}(\vec{r}) = \frac{\mu_0}{4\pi} \int_V \vec{M}(\vec{r}') \times \frac{(\vec{r}-\vec{r}')}{|r-r'|^3} d\sigma'$$

$$= \frac{\mu_0}{4\pi} \int_V \frac{\vec{j}_M(\vec{r}')}{|r-r'|} d\sigma' + \frac{\mu_0}{4\pi} \int_S \frac{\vec{j}_{ix}(\vec{r}')}{|r-r'|} da'$$

as you expect from B-S law.

d) Now $\vec{B} = \vec{B} \times \vec{A}$ so

$$\vec{B}(\vec{r}) = \mu_0 \vec{M}(\vec{r}) - \mu_0 \vec{\varphi}^*(\vec{r})$$

$$\vec{\varphi}^*(\vec{r}) = \frac{1}{4\pi} \int_V \frac{\vec{M}(\vec{r}') \cdot (\vec{r}-\vec{r}')}{|r-r'|^3} d\sigma'$$

e.) In general when we have ext. currents also

$$\vec{B}(\vec{r}) = \frac{\mu_0}{4\pi} \int_V \frac{\vec{j}(\vec{r}') \times (\vec{r}-\vec{r}')}{|r-r'|^3} d\sigma' + \mu_0 \vec{M}(\vec{r}) - \mu_0 \vec{\nabla} \vec{\varphi}^*(\vec{r})$$

But we need $\vec{M} = \vec{M}(\vec{B})$ So introduce

get
Next
page
 $\vec{B} = \mu_0 \vec{H}$
 $\vec{J} \times \vec{B} = \mu_0 \vec{J} + \mu_0 \vec{M}$

e.) The magnetic intensity \vec{H}

$$\vec{H} = \frac{1}{\mu_0} \vec{B} - \vec{M}, \quad \text{but still } \vec{q}^* \text{ depends on } \vec{M}$$

let's try differential approach to relate \vec{H} directly to \vec{J} !

$$1) \nabla \cdot \vec{B} = 0$$

$$2) \nabla \times \vec{B} = \mu_0 (\vec{J} + \vec{J}_M) \quad \vec{J}_M = \nabla \times \vec{M}$$

$$S_2 \Rightarrow \boxed{\nabla \times \vec{H} = \vec{J}}$$

Ampere's law in presence
of mag. material.

$$S_2 \quad \boxed{\oint_C \vec{H} \cdot d\vec{l} = I_{ext}}$$

free or ext. current
only.

f.) Linear, isotropic Mag. material:

$$\vec{M} = \chi_m \vec{H}$$

χ_m mag. susceptibility.

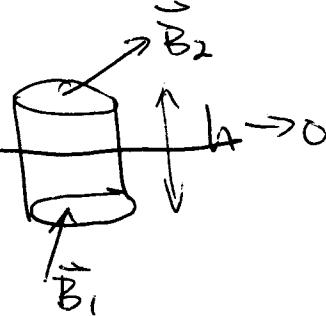
$$\Rightarrow \vec{B} = \mu_0 (1 + \chi_m) \vec{H} \equiv \mu \vec{H}$$

μ permeability.

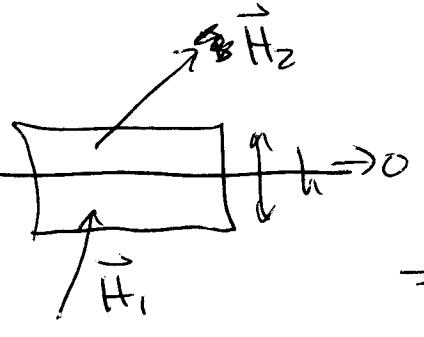
$$K_m = \frac{\mu}{\mu_0} = 1 + \chi_m$$

K_m relative permeability.

\times g.) B.C.

1) 

$$\nabla \cdot \vec{B} = 0 \Rightarrow B_{z_n} = B_{1n}$$

2) 

$$\oint \vec{H} \cdot d\vec{l} = I \Rightarrow H_{2t} = H_{1t} \quad (\text{no surface currents})$$

h.) BVP : 1) $\nabla \cdot \vec{B} = 0$
 2) $\nabla \times \vec{H} = 0 \Rightarrow \vec{H} = -\nabla \varphi^*$

$$\begin{cases} 1) \vec{B} = \mu \vec{H} \text{ linear} \Rightarrow \nabla \cdot \vec{H} = 0 \\ 2) \nabla \cdot \vec{M} = 0 \text{ uniform } \vec{M} \Rightarrow \nabla \cdot \vec{H} = 0 \end{cases}$$

$$\Rightarrow \nabla^2 \varphi^* = 0 \quad \text{Laplace eq.} \\ + \text{B.C.} \quad \underline{\underline{=}} \quad \text{BVP.}$$

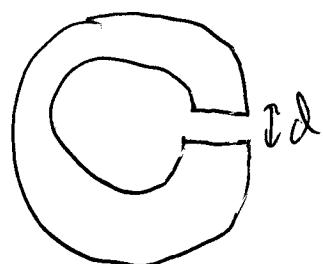
i.) Problems with known current distributions:

1.) Torus with N turns & I linear material



$$\oint \vec{H} \cdot d\vec{l} = I \Rightarrow H = \frac{NI}{2\pi r} \Rightarrow B = \mu \frac{NI}{2\pi r}$$

X. i) Torus with gear:



linear material $\vec{B} = \mu \vec{H}$

$$\oint_C \vec{H} \cdot d\vec{l} = NI + B_c l$$

$\Rightarrow B$ = same everywhere

$$B = \frac{\mu \mu_0 NI}{\mu_0 2\pi r + d(\mu - \mu_0)}$$

End of Statics

XI. Electromagnetic Induction: $\frac{\partial \vec{B}}{\partial t} \neq 0$.

a) $Emf = \mathcal{E} = \oint_C \vec{E} \cdot d\vec{l} \neq 0$ when $\frac{\partial \vec{B}}{\partial t} \neq 0$.

b) Faraday's law new exp. law: 1831

$$\mathcal{E} = - \frac{d\phi}{dt} \quad \phi = \int_S \vec{B} \cdot d\vec{S} \quad \text{integral form}$$

$$\vec{\nabla} \times \vec{E} = - \frac{\partial \vec{B}}{\partial t} \quad \text{diff. form.}$$

(- sign = Lenz's law)